CALIFORNIA COASTAL COMMISSION

CENTRAL COAST DISTRICT 725 FRONT STREET, SUITE 300 SANTA CRUZ, CA 95060 PHONE: (831) 427-4863 FAX: (831) 427-4877 WEB: WWW.COASTAL.CA.GOV



F18a

3-23-0014 (GROSSMAN ARMORING) FEBRUARY 10, 2023 HEARING EXHIBITS

- Exhibit 1 Location Maps
- Exhibit 2 View looking downcoast from Florin Street Overlook
- Exhibit 3 California Coastal Records Project photos of the site from 1972 to 2019
- Exhibit 4 April 2020 plans (showing undercut bluff and then-proposed emergency fill)
- Exhibit 5 March 2022 as-built plans (showing new fill and seawall constructed under G-3-20-0025, G-3-21-0023, and G-3-21-0035)
- Exhibit 6 August 2021 plans (showing proposed Phase IIB work)

Exhibit 7 – February 2022 plans (showing additional proposed downcoast seawall work)

- Exhibit 8 May 2005 plans showing nine unpermitted tiebacks
- Exhibit 9 February 2022 Applicant photos of armoring completed under G-3-21-0035
- Exhibit 10 2005 Staff photos of unpermitted house construction work
- Exhibit 11 Applicant's 2005 calculations for house construction work
- Exhibit 12 January 2023 Staff Sand Supply Impacts Memorandum



Regional Location Map

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Project Location

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Project Location

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Source: Google Earth, 2019

View looking downcoast at project site from Florin Street Overlook

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California Coastal Records Project Photo - 1972

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California Coastal Records Project Photo - May 1979

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California Coastal Records Project Photo - January 1989

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California Coastal Records Project Photo - September 2002

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California Coastal Records Project Photo - October 2004

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California Coastal Records Project Photo - September 2010

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California Coastal Records Project Photo - September 2015

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California Coastal Records Project Photo - October 2019

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North

EXPLANATION



Horizontal landward extent of wave action undercutting (plan view)



Seaward bottom of wave action undercutting (plan view)

Seaward top of wave action undercutting (plan view)

Note: Topographic contours at 2-foot intervals based on NAVD88 vertical datum using GPS surveyed stations. Topography determined from GPS and Drone Photogrammetric surveys performed on 03/23/2020 - 03/24/2020 by Cotton, Shires and Associates, Inc. Bluff undercut survey conducted on 03/23/2020 by Cotton, Shires and Associates, Inc. using measuring tape, laser distance meter, and GPS survey methods. Property lines from 07/03/2020 survey by Golden State Aerial Surveys, inc.



3-23-0014 Exhibit 4 Page 1 of 4 Approximate Location of Property Line, typ.

COTTON, SHIRES AND ASSOCIATES, INC CONSULTING ENGINEERS AND GEOLOGISTS				
SITE TOPOGRAPHIC AND BLUFF UNDERCUTTING PLAN IMMEDIATE MITIGATION OF BLUFF UNDERCUTTING				
121 INDIO DRIVE				
PISMO BEACH, CALIFORNIA				
GEO/ENG BY	SCALE	PROJECT NO.		
TRH	1"=10'	E0222L		
APPROVED BY POS	DATE April 2020	FIGURE NO. 2		

Section 1-1'

Section 2-2'

-60

ELEVATION (feet)

ELEVATION (feet)

-20



ELEVATION (feet)

60-

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Section 3-3'







North





Horizontal landward extent of wave action undercutting (plan view)



Seaward bottom of wave action undercutting (plan view)

Seaward top of wave action undercutting (plan view)

20 10 (feet)



Approximate Location of Property Line, typ.

COTTON, SHIRES AND ASSOCIATES, INC CONSULTING ENGINEERS AND GEOLOGISTS				
PHASE I - SHOTCRETE/CONCRETE/GROUT INFILL PLAN IMMEDIATE MITIGATION OF BLUFF UNDERCUTTING				
121 INDIO DRIVE				
PISMO BEACH, CALIFORNIA				
GEO/ENG BY	SCALE	PROJECT NO.		
TRH	1"=10'	E0222L		
APPROVED BY POS	DATE April 2020	FIGURE NO. 5		







Section 3 line extends an additional 51.5' to the NE

Section 5 line extends an additional 53.0' to the NE

(E) Remnant of 2005 return wall. Only the footing of the wall remains in this location

As-Built (2022) Location of the Seaward -Contoured, Textured, Concave, and 'Midnight" Coloration Facing of the Emergency Replacement Cutoff Wall and Upcoast and Downcoast Return Walls, based on GPS surveys performed in March 2022 by Cotton, Shires and Associates, Inc.

> Note: As-Built Emergency Replacement (2022) Cutoff Wall Extends 4' Laterally as the Recurved Upcoast and Downcoast Return Wall and Into Adjacent Pismo Formation Bedrock at each End

Recommended Shotcrete Cut-off Wall and Upcoast, Downcoast Return Walls on Design Drawings (CSA, 2020, 2021)

3

6

(E) (2005) Cutoff Wall, Eroded and Undercut by Marine Erosion after 2018 - Shotcrete Infill

- Approximate Location of Property Line, typ.

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	/		
Note: Restoration of the bluff drainage system and construction of contoured, textured, and color harmonized bluff shotcrete facing with tiebacks, and limited excavation of oversteepened Terrace Deposits, above the downcoast cutoff wall segment, will be implemented in coordination with the construction of bluff protective works proposed by others on adjacent 117 Indio Drive as Phase IIB.			
125 Indio D	rive		Seawall
As-built location of 2005 shotcrete cu GPS and Drone F surveys performe 03/24/2020 by Co Associates, Inc.	of seaward e utoff wall bas Photogramm ed on 03/23/2 otton, Shires	App full edge of sed on etric 2020 - and	roximate water prior
EXPLANATION Horizontal landward exten action undercutting (plant)	t of wave view)	Note: Notc shotcrete o height and adjacent so into Pismo bedrock at each en	h (N) Phase cutoff wall fu depth as egment 4' la Formation d.
			COTTON, SHIRES
		Patrick (DESIGNED	O. Shires, P.E. 10-1 DA

BY DATE APP'D

CHECKED

DATE

REVISIONS

All work still to be completed highlighted in blue





All work still to be completed highlighted in blue

SS SEC	SOCIATES, INC. DLOGISTS	PROFESSION	330 Village Lane Los Gatos, California 95030 (408) 354-5542 Fax: (408) 354-1852		Mr. Gary Grossman T Gary H. Grossman Tr P.O. Box 13
20	SUBMITTED:	Le RICK O. SHIPPE			Pismo Beach, CA (805) 556-3060
		NO. 26397 WE THOSE AND	APPROVAL:		
- F			4		







Page 2 of 2



Drone aerial photo sequence (late afternoon direct sunlight/dried shotcrete conditions, February 3, 2022) of ECDP G-3-21-35 emergency replacement cutoff wall [rCOW] and upcoast/downcoast return walls [RW] after completion of construction: Upper left: In Area 1, reduced height, textured, concave, dry "Midnight" and Tmp-harmonized coloration, recessed RW, locally w/mineralization, groundwater exfiltratation (upcoast STA 0+84' to STA 0+80'); in Area 2, reduced height, textured, concave, "Midnight" and dry Tmp-harmonized coloration rCOW, along the varied downworn back beach plane Tmp (STA 0+80' to STA 0+60'), locally w/mineralization, groundwater exfiltratation, looking n'e'ly. Upper right: In Area 1, reduced height, textured, concave, dry "Midnight" and Tmp-harmonized coloration, recessed RW; in Area 2, contoured, textured, concave rCOW (STA 0+80'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and dry Tmp-harmonized coloration rCOW (STA 0+60'); in Area 3, reduced height, textured, concave, sunlight-reflecting "Midnight", and textured, concave, sunlight-reflecting "Midnight", a back beach plane Tmp and head-cutting erosional channels, looking e'n'e'ly. Lower left: In Area 2, varied height, textured, concave, dry "Midnight" and Tmp-harmonized coloration rCOW; in Area 3 (near STA 0+58' to 0+26') and Area 4 (STA 0+26' to shown 0+16') conformed to varied downworn back beach plane Tmp, head-cutting erosional channels, and adjacent beach sand coloration, looking n'n'e'ly. Lower right: In downcoast Area 3, reduced height, textured, contoured, "Midnight" coloration rCOW (STA 0+39' to 0+29'); in downcoast Area 4 (STA 0+19' to 0+4'), full height, textured, contoured, rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, adjacent accreted beach sand; and in Area 5 (STA 0+4' to 0+0'), full height, textured, contoured rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, adjacent accreted beach sand; and in Area 5 (STA 0+4' to 0+0'), full height, textured, contoured, rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, adjacent accreted beach sand; and in Area 5 (STA 0+4' to 0+0'), full height, textured, contoured, rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, adjacent accreted beach sand; and in Area 5 (STA 0+4' to 0+0'), full height, textured, contoured, rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, adjacent accreted beach sand; and in Area 5 (STA 0+4' to 0+0'), full height, textured, contoured, rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, adjacent accreted beach sand; and in Area 5 (STA 0+4'), full height, textured, contoured, rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, adjacent accreted beach sand; and in Area 5 (STA 0+4'), full height, textured, contoured, rCOW, w/"Midnight" coloration, mineralization, groundwater exfiltration, groundwater exfiltr tion, mineralization, substantial groundwater exfiltratation, accreted adjacent beach sand, and e'ly of STA 0+0', the newly prograded downcoast sea cave, w/horizontal joints ("HJ") & overhanging highly fractured Tmp, looking n'ly.



Exhibit 5. Post-Emergency Replacement Cutoff Wall and Return Walls Construction Site Conditions; DA, 20220325.

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Upper left: Sun-dried "Midnight" coloration, concave, textured, reduced height RW (STA 0+84' [1] to 0+80' [2], rCOW contoured along Tmp outcrop (STA 0+80' [2] to 0+78' [3]), w/mineralization [4], exfiltrating groundwater [5], accreting beach quality sand and pebbles [6], looking e'n'e'ly.

Upper left center: Sun-dried "Midnight" coloration, Upper right center: W'ly-facing "Midnight" coloraconcave, textured, reduced height rCOW (STA 0+ 79' [7] to 0+72' [8], looking n'ly.

tion, concave, textured, reduced height rCOW (STA 0+63' [9] to 0+60' [10], contoured to Tmp [11], looking s'ly at the Pismo-Guadalupe Dunes [12].

Lower left: S'w'ly-facing "Midnight" colora- Lower left center: S'w'ly-facing "Midnight" coloration, textured, reduced height looking n'n'w'ly to the Irish Hills [17].

tion, concave, tectured rCOW (STA 57 [16], rCOW (STA 0+56' [18] to 0+38' [19], contoured to back beach Tmp, erosional Lower right center: Detail of concave rCOW Lower right: S'ly-facing Tmp contured [23], textured, "Midnight" coloration rCOW (STA channels [20], w/groundwater exfiltratation [21], mineralization [22], looking e'ly. facing (19a), Tmp contour (20a), STA 0+38'. 0+36' [24], 0+26' [25], 0+18' [26], recent wave runup [27], accreted sand [28], looking n'ly.



Exhibit 5. Post-Emergency Replacement Cutoff Wall and Return Walls Construction Site Conditions; DA, 20220325.

Upper right: S's'w'ly-facing "Midnight" coloration, concave, textured, reduced height rCOW (STA 0+59' [13] to near 0+43' [14], contoured to back beach Tmp terrain, erosional channels [15], looking n'ly.

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Exhibit 5. Post-Emergency Replacement Cutoff Wall and Return Walls Construction Site Conditions; DA, 20220325.

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2005 Staff Photo of Unpermitted Demolition and Construction at 121 Indio Drive

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2005 Staff Photo of Unpermitted Demolition and Construction at 121 Indio Drive

3-23-0014 Exhibit 10 Page 2 of 2

EXHIBIT 4

STRUCTURAL CALCULATIONS AND ELEVATIONS REPAIR AND MAINTENANCE OF SINGLE-FAMILY HOME 121 INDIO DRIVE, PISMO BEACH (GROSSMAN)¹

Prepared by LGA/LEONARD GRANT, ARCHITECT:²

) exterior walls, in lineal feet (LF): ³	294.3 LF
Is removed for replacement:	143.2 LF
cement: cement:	48.7%
	33.8%
nce work involved no change ndation (building footprint).	
<u>SSOCIATES</u> ⁵	
er (pre-project), in lineal feet: 6	279.5 LF
94.2 feet	
49.3 feet	
49 feet	
87 feet	
er removed for replacement:	133.4 LF
36.7 feet	
16.5 feet	
33.5 feet	
46.7 feet	
terior walls removed for replacement: ⁷	47.7%
) exterior walls, in lineal feet (LF): ³ Is removed for replacement: ⁴ eal footage exterior walls cement: isting home removed for <u>nce work involved no change</u> <u>idation (building footprint).</u> <u>SSOCIATES⁵</u> er (pre-project), in lineal feet: ⁶ 94.2 feet 49.3 feet 49 feet 87 feet er removed for replacement: 36.7 feet 16.5 feet 33.5 feet 46.7 feet

1 Prepared by Stephanie Dall, Dall & Associates, February, 2005 from information as noted.

2 February, 2005. LGA is the architect to Mr. Grossman for the repair and maintenance project.

4 Includes window space.

5 Dall & Associates (D&A) is the coastal consultant to the Gary H. Grossman Trust (Gary Grossman, Trustee), owner of the home and property at 121 Indio Drive, Pismo Beach. D&A's calculations (February, 2005) are based on to-scale elevations prepared by the Robert Richmond Company Architects, which were field-checked on 2/11/05, and have been compared to California Coastal Records imagery for confirmation of spatial accuracy.

6 Includes window space. Measurements did not include the column perimeters in the exterior facade that were apparently included by LGA.

7 Includes window space.

³ Includes window space.

STRUCTURAL CALCULATIONS AND ELEVATIONS REPAIR AND MAINTENANCE OF SINGLE-FAMILY HOME 121 INDIO DRIVE, PISMO BEACH (GROSSMAN)

Prepared by DALL & ASSOCIATES, cont'd.:

4. Exterior walls (pre-pro	oject), in square feet (SF):	2,910.9 SF		
Front:	891.2 sq. ft.			
North (right):	587.6 sq. ft.			
South (left):	566.5 sq. ft.			
Rear:	865.6 sq. ft.			
5. Exterior walls remove	d for replacement:	1 194 2 SE		
Front:	336.3 sg. ft.	1,104.201		
North (right):	151.6 sg. ft.			
South (left):	303.2 sg. ft.			
Rear:	403.1 sq. ft.			
	·			
6. Percentage of total ex	terior walls removed for replacem	ent: 41.0%		
7. Foundation perimeter	(pre-project), in lineal feet (LF):	280 LF		
8 Foundation perimeter	reinforced or removed			
and ranks and 8				
and replaced.		29 LF		
9 Equipartian total aubia				
and replaced in o	valus repaired or removed			
and replaced, in ci		1.2 CY		
10. Percentage of total for	undation removed and replaced:	10.3%		
The repair and maintenar	ice work involved no change			
in the location of the foun	dation (building footprint)			

8 Also reflected in the exterior wall "removed" calculations, broken out here for further clarity.

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CALIFORNIA COASTAL COMMISSION 455 MARKET STREET, SUITE 228 SAN FRANCISCO, CA 94105-2219 VOICE (415) 904-5200 FAX (415) 904-5400



January 26, 2023

SAND SUPPLY IMPACTS MEMORANDUM

To: Katie Butler, Coastal Program Supervisor

- From: Jeremy Smith, Coastal Engineer Joseph Street, Ph.D., P.G., Staff Geologist
- Re: 121 Indio Drive, Pismo Beach (Grossman Property), CDP application 3-23-0014

The purpose of this memorandum is to assess the adverse impacts of the proposed armoring associated with the above-referenced site and CDP application on shoreline sand supply, and therefore, on public access and recreational opportunities.

To this end, we have reviewed the following documents provided by the Applicant:

- Cotton, Shires and Associates, Inc., 2020, "Maintenance/Repair Phase I Geotechnical Investigation Report", dated March 31, 2020, signed by P.O. Shires and J.M. Wallace.
- Cotton, Shires and Associates, Inc., 2020, "Maintenance/Repair/Restoration -Phase I Geotechnical Investigation Report Update", dated April 6, 2020, signed by P.O. Shires and J.M. Wallace.
- Cotton, Shires and Associates, Inc., 2021, "Calculation of Projected Volumes of Beach Quality Sand Production During 20 Years at 121 Indio Drive Without Phase I and Phase II Development", dated February 17, 2021, signed by P.O. Shires and J.M. Wallace.
- 4) Cotton, Shires and Associates, Inc., 2022, "As-Built Emergency Replacement Cutoff Wall and Upcoast, Downcoast Return Walls", site plan dated March 2022.
- 5) Cotton, Shires and Associates, Inc., 2022, "Emergency Replacement Cutoff Wall and Minor Cutoff Wall/Return Wall Extension (ECDP G-3-21-0035) – Condition 10 Checklist", dated March 25, 2022, signed by P. Shires.

In addition, we have consulted several other documents providing geologic information relevant to the project site and vicinity:

- TerraCosta Consulting Group, Inc., 2020, "Coastal Bluff Evaluation and Geotechnical Basis of Design, Bluff Stabilization Project, 117 Indio Dr., Pismo Beach, California", Dated September 10, 2020, signed by W.F. Crampton and B.R. Smillie.
- 7) California Coastal Commission Adopted Findings, Coastal Development Permit A-3-PSB-02-016, approved August 6, 2003.

 Cotton, Shires and Associates, Inc., 2003, "Geotechnical Investigation Potential Seacliff Hazards, 121 and 125 Indio Drive and Florin Street Cul-De-Sac, Pismo Beach, California, dated January 2003.

Coastal Act Section 30235 allows for shoreline armoring in specific cases "when designed to eliminate or mitigate the adverse impacts on shoreline sand supply". In the present case, adverse effects from proposed armoring, including fixing the back beach, encroaching on potential beach space, and preventing the natural supply of beach-quality sand cannot be eliminated, and thus must be adequately mitigated.

Three of the effects due to shoreline armoring can be quantified: 1) loss of the beach area on which the structure is located (encroachment); 2) the long-term loss of beach which will result when the back beach location is fixed on an eroding shoreline (passive erosion); and 3) the amount of sand-generating material which would have been supplied to the beach if the back beach or bluff were to erode naturally (sand retention). Passive erosion and sand retention are in part based on the assumed rate of retreat in the absence of armoring. As is discussed in more detail in the section "Bluff Retreat Rate", we calculated impacts for a range of retreat rates: one foot per year, considered to be a likely mid-range estimate, and two feet per year, considered to be a conservative estimate.

Encroachment and passive erosion are assessed as areas (square feet), where the former represents the area under the armoring itself (i.e., its footprint on the beach) and the latter represents the area of future beach that would be naturally created if not for the fixing of the shoreline. Sand retention is assessed as a volume of sand (cubic yards) that would enter the littoral system but for the fixing of the shoreline. In-kind mitigation would involve creating the equivalent amount of beach area and placing the equivalent volume of sand into the littoral system. In-lieu mitigation involves paying compensatory fees and/or providing compensatory improvements to enhance coastal resources (typically in the form of public access and recreation improvements) of similar monetary value.

The Commission has used a variety of methods to evaluate these areas and volumes for in-lieu mitigation fees. The methods used here are fairly standard and representative of the Commission's approach to such impact assessment and mitigation, and involve 1) the use of a real estate valuation method for the calculated encroachment and passive erosion areas in which the cost of acquiring property nearby that could be purchased and allowed to erode and turn into similar beach naturally is applied (dollars per square foot); and 2) for the retained sand volume, the cost of purchasing and transporting beach quality sand to the project vicinity is applied (dollars per cubic yard of sand).

In this case, and as detailed more specifically below, the total calculated impacts on sand supply, and therefore, on public access and recreational opportunities are assessed to be 1,120.29 to 2,268.58 cubic yards of retained sand, 236 square feet of encroachment, and 1,610 to 3,220 square feet of passive erosion. Using a cost of sand of \$60.54 per cubic yard and a cost of property acquisition of \$450.25 per square foot, **the total range of a potential in-lieu fee calculated is \$898,984 to \$1,693,404** (rounded to the nearest dollar).

The following section elaborates on the values used in this assessment.

Encroachment

Encroachment considers the amount of beach space taken up by a shoreline protection device. Using the Applicant's March 2022 As-Built Plans, the area (looking from plan view) of the as-built emergency replacement cutoff wall and upcoast and downcoast return walls, including the roughly four feet of remnant footing of the 2005 return wall, proposed to remain as part of this project, as well as a 13 foot long, 2 foot wide cutoff wall extension proposed as part of this project was calculated using the measure tool in Adobe Acrobat to be approximately 236 square feet. Note, the footprint of the sea cave infill is not included in the encroachment calculation because that area is effectively captured by the passive erosion calculation below.

 $A_e = 236$ square feet

Passive Erosion

Passive erosion considers the amount of beach that would be created over time through natural erosion processes if not for the effects of the proposed shoreline protection device, which will fix the back of the beach (i.e., here, the toe of the bluff) in its current position. To estimate a yearly value, the expected average annualized erosion rate (feet per year) and the width of the shoreline protection device (feet) are multiplied together.

$$A_w/year = R * W$$

The width of the structure was determined by Cotton, Shires, and Associates, Inc. (CSA, Ref. 3) to be 70 feet. We confirmed this to be an appropriate estimate of the alongshore width. We determined the appropriate retreat rate over this period to be one foot per year, approximately double the Applicant's consultant's estimate. Our rationale is described in the "Retreat Rate" section on page four. Therefore, the amount of passive erosion was calculated to be 70 to 140 square feet per year.

 $A_w/year = 1.0 * 70 = 70$ square feet/year $A_w/year = 2.0 * 70 = 140$ square feet/year

Consistent with the Commission's experience that shoreline armoring often needs to be reinforced, augmented, replaced, or substantially changed within twenty years of its original installation, and to provide for re-review on a regular basis to allow for consideration of possible changes in policy, law, and physical conditions associated with armoring, the Commission typically applies an initial twenty-year period from the date of approval as its initial mitigation window. Thus, mitigation is assessed and applied in time increments, where impacts past the first timeframe are not quantified here, but would be required to be quantified, and commensurate mitigation provided, if the proposed armoring were to be in place past the initial mitigation period. In this case, the typical twenty-year time frame was elongated slightly because the armoring has been in place (and therefore adversely impacting coastal resources) for approximately three years. Thus, the assessment period was determined to be 23 years. And therefore, the amount of passive erosion over 23 years was calculated to be 1,610 to 3,220 square feet.

Sand Retention

Sand retention considers the amount of beach quality sand that is prevented from entering the littoral system through bluff/shoreline erosion as a result of the shoreline protection device. To estimate this, the expected average annualized erosion rate (feet per year), the width of the shoreline protection device (feet), and the height of the bluff (feet) are

multiplied together and then converted from cubic feet to cubic yards to establish a yearly impact value. This represents the amount of bluff material being retained by the structure on average per year. Because beaches are primarily made of sand, an assumed bluff sand fraction is determined and multiplied by the volume to estimate the amount of material that is beach quality sand. If the shoreline protection device is not anticipated to halt the erosion of entire bluff face, but instead allows for retreat of the upper bluff, an adjusted formula can be used to account for the pro-rated amount of bluff that may continue to erode. The proposed project is anticipated to halt the erosion of the full bluff face and so this adjusted formula does not apply.

$$V_b/year = S * (R * W * h_s) * \frac{1}{27}$$

The "beach compatible" sand fractions estimated by CSA in its 2/17/2021 sand supply impact analysis (Ref. 3) were 8% for the Pismo Formation bedrock and 7.3% for the Terrace Deposits based on their grain-size analysis of the sand present on the beach below the project site. It is important to recognize, however, that due to the relatively high wave energy at the site only the coarser fractions of the sand present in the bluff remain on the beach, with the rest carried offshore or downdrift. In their 2003 report (Ref. 8), CSA found that 40% of the Pismo Formation bedrock and 54% of the Terrace Deposits would degrade to sand-sized particles. The latter estimates represent the full sand fraction, which is often used by the Commission in evaluating sand retention impacts. The fine and medium sized sand particles perform an important role in the offshore (submerged) portions of the beach, as well as within the larger littoral cell; fine- and medium-grained sand is transported downdrift and deposited on other beaches nearby. Using the approximate ratio of Pismo Formation to Terrace Deposits, a weighted-average sand fraction was determined to be approximately 0.49 (i.e., 49 percent sand). We used the same alongshore width of armoring of 70 feet, the expected average annual bluff retreat rate of 1.0 feet per year, and initial mitigation assessment period of 23 years. For the height, the full height of the bluff was used since the project is intended to halt the erosion of the full bluff. This was estimated by CSA (Ref. 3) to be 39.3 feet. These parameters are summarized below:

When multiplied together and converted to cubic yards, the estimated sand retained by the project is 1,148.29 cubic yards or approximately 1,148 cubic yards.

$$V_b = 0.49 * (1.0 * 23 * 70 * 39.3) * \frac{1}{27} = 1,148.29 \text{ cubic yards}$$

$$V_b = 0.49 * (2.0 * 23 * 70 * 39.3) * \frac{1}{27} = 2,296.58 \text{ cubic yards}$$

Prior to the emergency work at the site, an extensive sea cave formed as a result of erosion of the bedrock material at the base of the bluff. Because the analysis above assumes this material to still be present, the volume of sand eroded should be subtracted from the total theoretical volume of sand retained. CSA estimated the volume of the eroded sea cave to be approximately 70 cubic yards (Ref. 3). Using the sand fraction for the Pismo formation bedrock of 40%, this equates to 28 cubic yards of sand. Additionally, the proposal includes approximately 20 cubic yards of excavation of the upper bluff to install stability improvements. This volume of material is effectively captured in the sand retention estimates. The project should maximize the beneficial use of excavated material to the extent any suitable material can be placed on the beach.

Therefore, the total amount of sand retained by the project, accounting for sand already lost to erosion, is 1,120.29 to 2,268.58 cubic yards.

Bluff Retreat Rate

As noted above, an estimate of the bluff retreat/erosion rate (*R*) is needed as part of the Commission's typical method for assessing the "passive erosion" and "sand retention" components of the sand supply impact of shoreline protection devices. On many occasions the Commission has used the estimated long-term annualized bluff erosion rate, based on historical observations, for this purpose. However, coastal bluff erosion is generally episodic in nature, and actual bluff retreat rates over short periods of time can vary substantially from the long-term average. When applied predictively to relatively short time periods, such as the approximate 20-year assessment period for sand supply impacts often used by the Commission, the long-term average rate is very likely to be "wrong", either overpredicting or underpredicting reality; use of a long-term rate is often justified, however, because of the difficulty of predicting the timing and magnitude of future episodic bluff retreat. Nonetheless, in situations where site-specific conditions or other evidence provide a reasonable basis for predicting future bluff erosion rates that differ from the long-term rate, greater or lesser rates can and should be used for evaluating hazards and the sand supply impacts of shoreline armoring.

The Applicant's sand supply impact analysis (CSA 2/17/2021, Ref. 3) estimated a longterm average annualized bluff retreat rate for the site based on an analysis of aerial photographs spanning the period 1955 – 2020. Within the Phase I and Phase IIA project areas, the bluff edge ("top of bluff") has retreated between 24 and 45 feet over this 65-year period, yielding an average annualized erosion rate of 0.54 feet per year (range 0.36 – 0.69 feet per year). On the southeastern (downcoast) portion of the bluff (Phase IIB project area), the estimated average erosion rate is 0.4 feet per year. The range in estimated erosion rates likely reflects both alongshore variability in the amount of erosion over this time period and normal, expected measurement error for this type of analysis.

For several reasons, however, we think it likely that the Applicant's long-term average annualized bluff erosion rate of 0.54 feet per year underestimates the rate of bluff erosion at the subject site over the next 20 years, assuming the site were left in an unarmored condition.

The 1955 - 2020 period assessed in the aerial photograph analysis includes long periods when large portions of the bluff were protected by armoring devices. Oblique aerial photographs from the California Coastal Records Project (http://californiacoastaline.org) indicate that the bluff face on the central portion of the site was covered with shotcrete/gunite at some point between 1979 and 1987 (possibly in the aftermath of the 1982-83 El Niño storms), and additional armoring, including a bluff toe seawall ("cut off wall") was added in 2004 - 2005 in association with a 2003 CDP. Although the bluff toe armoring has subsequently been penetrated and undermined by wave attack, the upper bluff protection remains largely intact. It is almost certain that these shoreline protection elements have, as intended, slowed bluff erosion over most of the period (41 out of 65 years) evaluated by CSA. Thus, the long-term erosion rate (1955 – 2020) provided by CSA reflects bluff erosion under natural conditions only for approximately 25 – 30 years, between 1955 and whenever the shotcrete was added in the 1980s, and very likely

underestimates the rate of erosion under natural, unarmored conditions. Given the uncertain timing and effectiveness of these prior armoring efforts, it is difficult to quantify their overall effect on the historical average annualized bluff erosion rate (0.54 feet per year) estimated by CSA. Nonetheless, if it is assumed that all the bluff retreat measured by CSA occurred during a 32-year period between 1955 – 1987, then the average annualized bluff retreat over this period would be 1.1 feet per year, twice as great as the CSA estimate.

- Since the construction of the bluff toe seawall in 2004 2005, wave attack at the base of the bluff has evidently been relatively intense, sufficient to destroy the base of the seawall and erode sea caves extending 7 27 feet into the Pismo Formation bedrock (CSA, Refs. 2 4). Even with the temporary protection provided by the seawall, this amount of undercutting yields bluff toe retreat rates of 0.47 1.8 feet per year between 2005 and 2020 (CSA reported an average of 12 feet of retreat, or 0.8 feet per year). Apparently, much of this erosion occurred since 2018 during stormy conditions. Recent bluff toe erosion rates thus generally exceed the long-term average rate proposed by the Applicant.
- The extensive undercutting and sea cave formation on the lower bluff effectively "sets up" future upper bluff failures, and thus relatively rapid retreat of the bluff edge and face in the near-term absent armoring. In previous reports, (e.g., Refs. 1 - 3), CSA concluded that upper bluff failures and rapid upper bluff retreat triggered by lower bluff erosion and sea cave collapse pose a significant, near-term threat to the blufftop residence, and this imminent danger was the primary justification for both several recent emergency CDPs issued by the Commission and for the proposed Phase I and II shoreline protective work (some of which has already been built). In our estimation, relatively rapid upper bluff retreat, potentially matching or exceeding the annualized rates (0.47 - 1.8 feet per year) observed recently in the lower bluff undercutting, is likely to occur within the next 20 years absent the proposed armoring.
- Recent high rates of bluff erosion are not confined to the project site, but have been observed elsewhere in the Shell Beach area. For example, TerraCosta (2020) (Ref. 6) reported 20 30 feet of retreat in the last 20 years (1 1.5 feet per year) along unarmored bluffs in Shell Beach, and concluded that a near-term retreat rate of 1.5 feet per year was applicable at 117 Indio Drive, immediately downcoast of the subject site. Prior to the construction of the 2005 seawall, short-term bluff retreat rates of up to 2 feet per year (1990 2000) were reported immediately upcoast at 125 Indio Drive (along with a retreat rate of 0.83 feet per year at 121 Indio Drive, likely lesser because the bluff there was already partially armored) and used as justification for the original seawall construction at the site (Gorman/ Earth Systems Pacific 2001 peer review, as cited in Ref. 7).
- Over the next several decades, it is widely predicted that rates of sea level rise along the California coast will increase above observed historical rates. Greater rates of sea level are expected to increase rates of retreat along coastal bluffs, and could result in more rapid erosion of the bluff at the project site.

For these reasons, we conclude that average annualized bluff retreat rates greater than 0.54 feet per year (as estimated by the Applicant) are very likely to occur at this location

over the next 20 years in the absence of further shoreline armoring. Based on the available evidence, we believe an erosion rate of 1 foot per year is likely, and that higher erosion rates of 1.5 to 2 feet per year are possible.

In-lieu Fee Calculation

Often, the Commission has determined that it is not practicable or appropriate to pursue inkind mitigation for sand supply impacts, and has instead required in-lieu mitigation. The Commission has used a variety of methods to translate area of beach lost (encroachment and passive erosion) and/or volume of sand retained to dollar amounts. As previously mentioned, the approaches used here are 1) the cost of acquiring property nearby that could be purchased and allowed to erode thereby turning into beach naturally (dollars per square foot); and 2) the cost of purchasing and transporting beach quality sand to the project vicinity (dollars per cubic yard of sand).

The cost of acquiring property nearby was estimated to be \$450.25 per square foot based property values in the project area. The cost of purchasing and transporting sand to the project vicinity was estimated to be approximately \$60.54 per cubic yard of sand based on the value of \$50 per cubic yard of sand used in similar projects in the area from 2017, adjusted for inflation to 2023 (using cumulative inflation rate for US Consumer Price Index). It is our understanding the basis for these values is to be elaborated on in the staff report.

Using these costs, the total impacts on sand supply, and therefore, on public access and recreational opportunities are assessed to be **1,120.29 to 2,268.58 cubic yards of retained sand, 236 square feet of encroachment**, and **1,610 to 3,220 square feet of passive erosion**. Using a cost of sand of \$60.54 per cubic yard and a cost of property acquisition of \$450.25 per square foot, **the total in-lieu fee calculated is \$898,984 to \$1,693,404** (rounded to the nearest dollar).

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