# **W11b**

# A-5-LGB-22-0025 (GRAY) April 12, 2023

## **EXHIBITS**

#### **Table of Contents**

Exhibit 1 – Project Location and Aerials of Project Site

Exhibit 2 - Project Plans

Exhibit 3 – Existing Retaining Walls

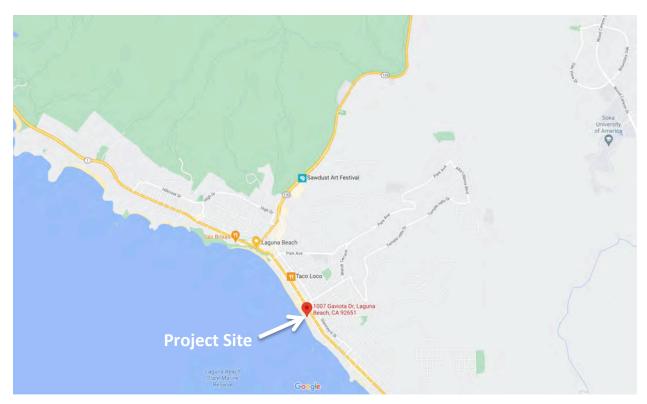
Exhibit 4 – Coastal Commission Bluff Edge Determination

Exhibit 5 – Bluff Edge and Geologic Setback Review Memorandum

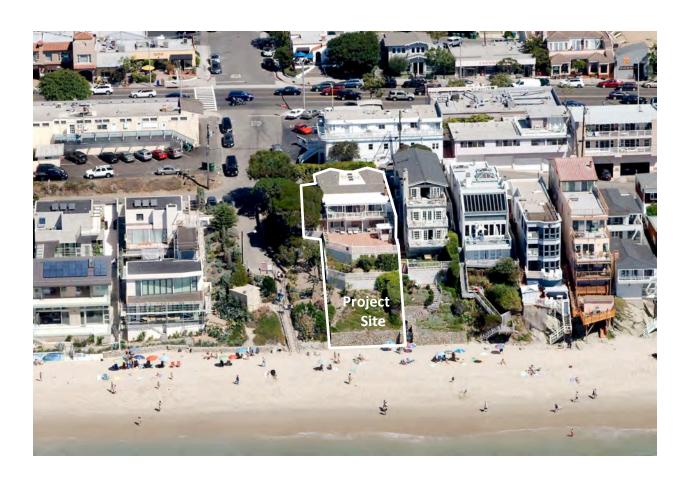
Exhibit 6 – Buildable Area

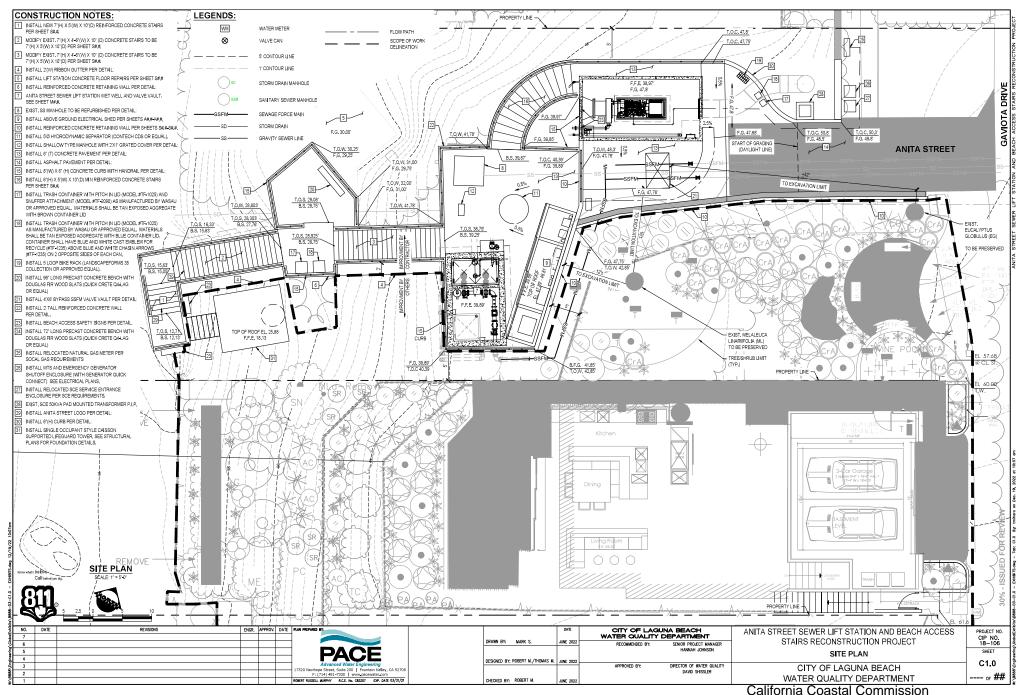
Exhibit 7 – 2014 Building Permit and Stop Work Order

Project Site: 1007 Gaviota Drive, Laguna Beach (APN: 644-076-01)









A-5-LGB-22-0025 Exhibit 2

Page 1 of 32

# Mike and Lori Gray Residence

1007 Gaviota Drive Laguna Beach, CA 92651



Abreviations	Symbols	Codes	Scope of Work	Project Data	Sheet Index
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31742 SOUTH COAST HIGHWAY LAGUNA BEACH CA 92651 TEL 949-307-0002

Milke and Lori Gray Residence 1007 Gaviota Drive Laguna Beach California 92651

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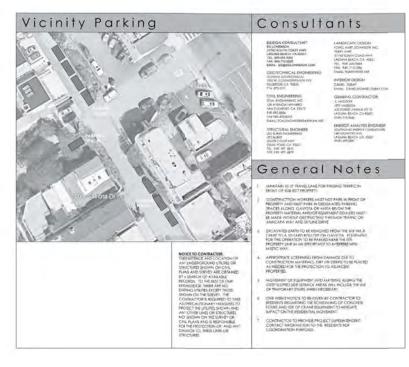
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California Coastal Commission

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- A COMPLETE SET OF THESE PLANS AND A COMPLETE SET OF LACUNA BEACH STANDARD DRAWNOS SHALL BE MAINTAINED ON THE JOB THROUGHOUT THE CONSTRUCTION.
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- AN APPROVED COPY OF THE GRADING PLAN SHALL BE ON THE PERMITTED SITE WHILE WORK IS IN PROCRESS.
- CUT AND FILL SLOPES SHALL BE NO STEEPER THAN 2-FOOT HORIZONTAL TO 1-FOOT VERTICAL (2-1) EXCEPT WHERE SPECIFICALLY APPROVED OTHERWISE.
- FILS SHALL BE COMPACTIO THROUGHOUT TO A MINIMAN OF ROE RELATIVE COMPACTION. ACCREGATE BASE FOR ASPHALTIC AMERIC SHALL BE COMPACTION IN A MINIMAN OF DOS RELATIVE COMPACTION. BANGING ICCOMPACTIVE OF A MINIMAN DEPOSIT SHALL BE CERTIMANDED BY CORT SHANGHOUND TO ICE ANYMOTOGO ECUMENTAL OF THE DESIRET BY LIVETON BUILDING COCK STANGHOUNG. OF 20 AMPROVED COUNTRICK.
- AREAS TO RECEIVE FILL SHALL BE PROPERLY PREPARED AND APPROVED I WRITING BY THE SOIL ENGINEER AND THE BUILDING OFFICIAL PRIOR TO FLADING FILL.
- FILLS SHALL BE BENCHED INTO COMPETENT MATERIAL PER DETAILS OR AS DIRECTED BY THE SOLS ENGINEER
- ANY EXSTING IRRIGATION LINES AND DISTERNS SHALL BE REMOVED, OR CRUSHED IN PLACE, AND APPROVED BY THE BULDING OFFICIAL AND SOLL PROMETE.
- STOCK PLING OF EXCESS MATERIAL SHALL BE APPROVED BY THE BUILDING OFFICIAL PRIOR TO EXCAVATION.
- THE DESIGN ENGINEER, AS A CONDITION OF ROUGH GRADE APPROVAL, SHALL PROVIDE A BLUE TOP MITH ACCOMPANYING WINESS STAME, SET AT THE CONTEX OF EACH FAIR REFERENCE THE PAIR DESIGNATOR FOR PRECISE PROMISE AND A BLUE TO WITH INTEREST STAMES SET AT THE DIMARACE STAME, BIGH POINT REFLICTING THE HIGH POINT REFLICTING THE PROBLEMANT PERMITS.
- ALL TRENCH BACKFILLS SHALL BE TESTED AND APPROVED BY THE SOLL ENGINEER FOR THE GRADING CODE.
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- PAVED STREETS, SICEWALKS, AND OTHER IMPROVEMENTS SHALL BE MAINTAINED IN A PANDS SEETER, SCHWALK, AND OTHER MEROMONISTS SHALL BE MANTHANG IN A MART AND CIEBA COMMITION FREE OF LOOSE SOIL, CONSTRUCTION CHEEKS, AND INSIGHT SERVICES OF CONTROL OF SHARL PROCESS OF CONTROL OF SHARL PANDS SHALL BE USED ON A SEED BASES TO PRIVATE CONTRICTION BRIDAY OF SISTEM FLOWER SHARLOW AND CERES SUSTBEE THE PROJECT BOUNDARDS. MATTERNS SHALL DAN'S BE USED TO CARE STREETS DEEPT WHEN ALL STORM DRAINS AND REACOURD AND MEN'S ALL REPORTS STREETS DEEPT WHEN ALL STORM DRAINS AND REACOURD AND MEN'S ALL REPORTS STREETS DEEPT WHEN ALL STORM DRAINS AND REACOURD AND MEN'S ALL REPORTS STREETS DEEPT WHEN ALL STORM DRAINS AND REACOURD AND MEN'S ALL REPORTS STREETS DEEPT WHEN ALL STORM DRAINS AND REACOURD AND MEN'S ALL REPORTS STREETS DEEPT WHEN ALL STREETS AND RESPONSE AND AND ALL REPORTS STREETS DEEPT AND MASS-MATTER MEN'S CHIEF THE STREET DRAIN.
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## lohrbach

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No. Date Revision 03.21.22

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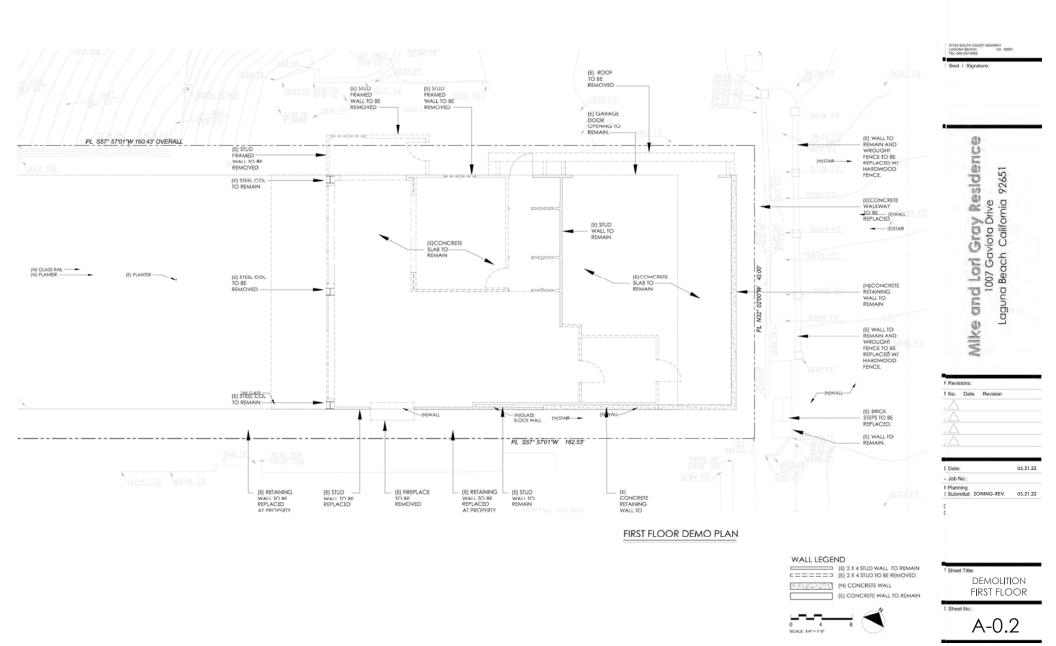
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STAGING PLAN

# lohrbach



California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 4 of 32

# lohrbach



# Mike and Lori Gray Residence 1007 Gaviota Drive Laguna Beach California 92651



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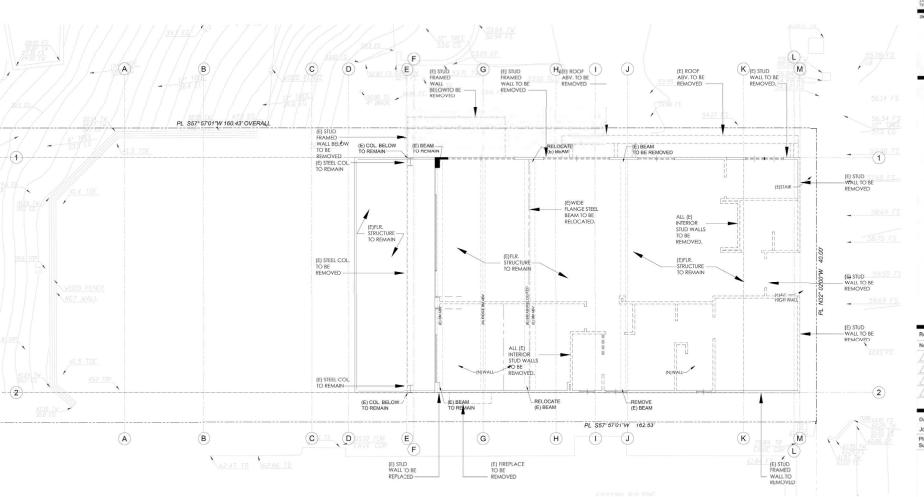
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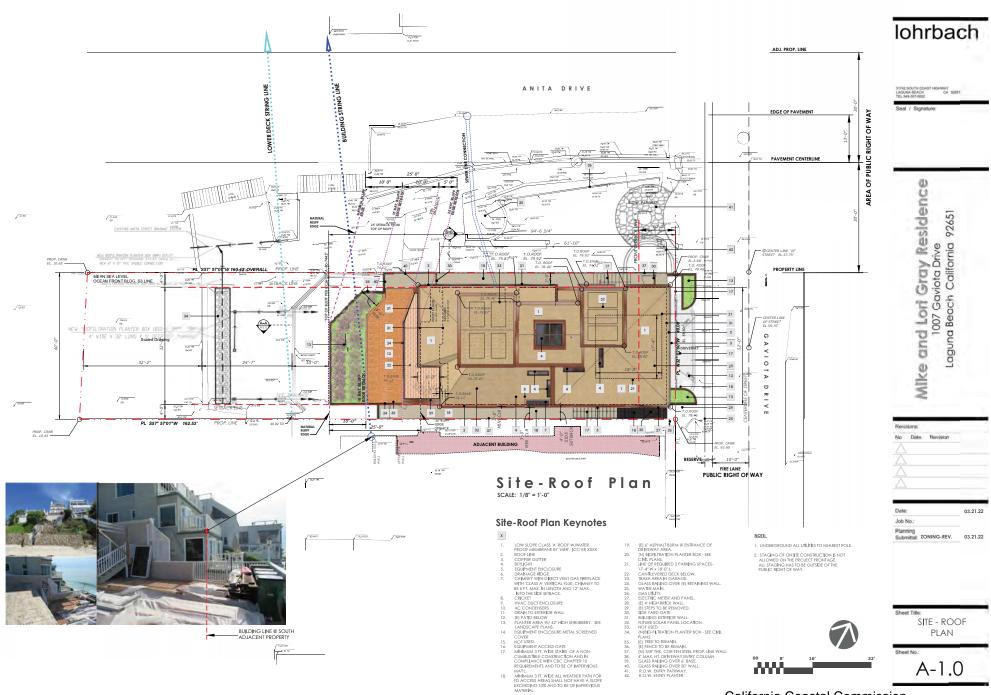
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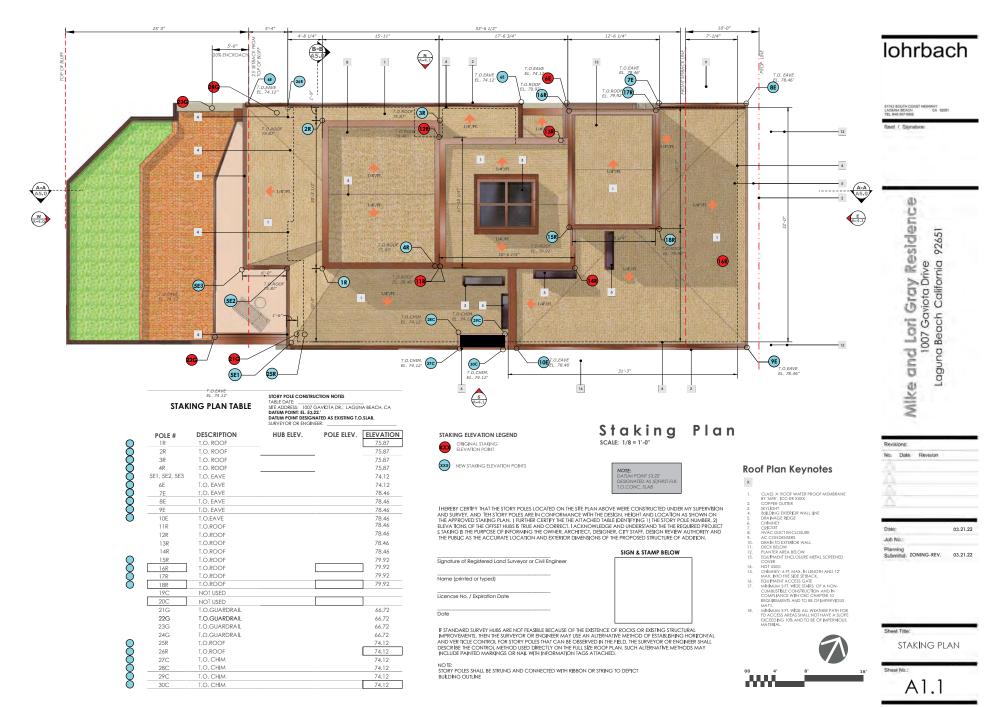
UPPER LEVEL FLCOR PLAN

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 5 of 32





California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 6 of 32



California Coastal Commission
A-5-LGB-22-0025
Exhibit 2
Page 7 of 32



#### First Floor & Basement Plan

#### **General Floor Plan Notes**

- REFER TO STRUCTURAL DRAWINGS FOR ALL FRAMING, BEARING AND SHEAR WALLS.
- 2 PENETRATIONS THROUGH THE WALL OR CEILINGS SEPARATING THE DWELLING PENE IRAJIONS I HEUGH HIE WALL OK CEIRNGS SEPAKAIJING THE DWELING UNIT FROM THE GARAGE SHALL BE FROTECTED IS SUCH AS THOSE FOR VENTS. PIPE, DUCTS, CABLES AND WIRES, WITH AND APPROVED MATERIAL TO REIST THE FREE PASSAGE OF FLAME AND PRODUCTS OF COMBUSTION, (CRC R302.5). DUCTS THROUGH GARAGE INTO DWELLING SHALL BE MINIMUM 26-GAILGE GALVANIZED STEEL.
- 3. THE CONTROL VALVES IN BATHTUBS, WHIRLPOOL BATHTUBS, SHOWERS AND THE SHOWER COMBINATIONS MUST BE PRESSURE BALANCED OF THERMOSTATIC MIXING VALVES. CPC SECTION 414.5 AND 418.0.
- ALL PLUMB IN FIXTURES SHALL BE COMPLY WITH THE MAXIMUM FLOW RATES
   AS NOTED IN THE RESIDENTIAL CONSTRUCTION MINIMUM REQUIREMENTS. SE
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#### Floor Plan Keynotes

- 224 WOOD FRAMING AT 16' O.C. PER C.R.C.
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  BUILDING PAPEP POS ELP-META CONCRETE SLAB
  INSULATION TRICOUGHOUT ALL PITERDOW WALLS AND FLOOR
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e and Lori Gray Residence 1007 Gaviota Drive Laguna Beach California 92651 Mike and

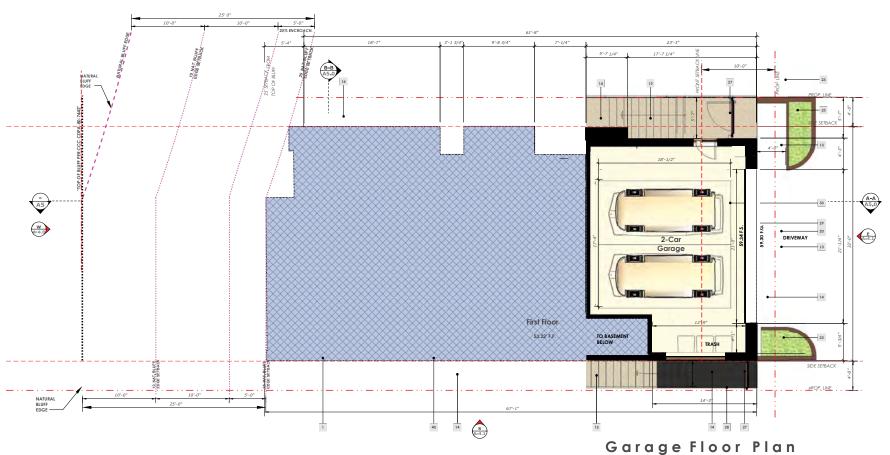
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FIRST FLOOR & **BASEMENT PLAN** 

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California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 8 of 32



#### **General Floor Plan Notes**

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  WATER CLOSE PITER' CYPSIAM BOADO AT ALL GRAAGE
  WALLS, CEILING AND UNDER STAMES. TAPE AND SAND,
  WATER CLOSE PITER OF STAMES AND AT ALL SAND SAND
  BY THE AMERICAN HAD THE STAME AND AND SET SAND
  SAND SET SAND ASSOCIATED RUSSHOMETER VALYES, F
  TEMPREED GASS SHOWER ENICLOSURE AND DOORTO
  6-07-AGOVE THE DRAIN. TOOR SHALL SWING OUT.
  TEMPREED GASS SHOWER ENICLOSURE AND DOORTO
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  DIAMETER CIRCLE.
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- IN CONDENSERTO HAVE, A SOUND ATTENUATED CONCRETE BLOCK ENCLOSURE TO MEET LACUIMA BEACH EXTERIOR NORSE EQUIEMENTS FOR A RESIDENCE, (7.25,400 DITENERS NORSE STANDARGS) (MEMBERSHEE CONSTRUCTION AND IN COMPUTACE WITH CECCHAPTER 10 REQUIREMENTS AND TO BE OF IMPERVIOUS MATL.)
- CONDITION OF THE CONTROL OF THE CONT

SCALE: 1/4" = 1'-0"

(N) CONC. REAINING WALL



e and Lori Gray Residence 1007 Gaviota Drive Laguna Beach California 92651 Mike and

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**GARAGE FLOOR** PLAN

A-2.1

California Coastal Commission A-5-LGB-22-0025

Exhibit 2 Page 9 of 32



#### Second Floor & Mezzanine Plan

#### SCALE: 1/4" = 1'-0"

#### **General Floor Plan Notes**

- REFER TO STRUCTURAL DRAWINGS FOR ALL FRAMING, BEARING AND SHEAR WALLS.
- 2 PENETRATIONS THROUGH THE WALL OR CEILINGS SEPARATING THE DWELLING PENE IRAJIONS I HEUGH HIE WALL OK CEIRNGS SEPAKAIJING THE DWELING UNIT FROM THE GARAGE SHALL BE FROTECTED IS SUCH AS THOSE FOR VENTS. PIPE, DUCTS, CABLES AND WIRES, WITH AND APPROVED MATERIAL TO REIST THE FREE PASSAGE OF FLAME AND PRODUCTS OF COMBUSTION, (CRC R302.5). DUCTS THROUGH GARAGE INTO DWELLING SHALL BE MINIMUM 26-GAILGE GALVANIZED STEEL.
- 3. THE CONTROL VALVES IN BATHTUBS, WHIRLPOOL BATHTUBS, SHOWERS AND THE SHOWER COMBINATIONS MUST BE PRESSURE BALANCED OF THERMOSTATIC MIXING VALVES. CPC SECTION 414.5 AND 418.0.
- ALL PLUMB IN FIXTURES SHALL BE COMPLY WITH THE MAXIMUM FLOW RATES
   AS NOTED IN THE RESIDENTIAL CONSTRUCTION MINIMUM REQUIREMENTS. SE
   SHEET GN-1 GENERAL NOTES.

#### Floor Plan Keynotes

- 224 WOOD FRAMING AT 16' O.C. PER C.R.C.
  W/DITERFOR WALL: //RE "EXTERIOR PLASTER OVER META
  BUILDING PAPEP POS ELP-META CONCRETE SLAB
  INSULATION TRICOUGHOUT ALL PITERDOW WALLS AND FLOOR
  PROVIDE SIZE PITERS' CYPSIAM BOADO AT ALL GRAAGE
  WALLS, CEILING AND UNDER STAMES. TAPE AND SAND,
  WATER CLOSE PITER' CYPSIAM BOADO AT ALL GRAAGE
  WALLS, CEILING AND UNDER STAMES. TAPE AND SAND,
  WATER CLOSE PITER' CYPSIAM BOADO AT ALL GRAAGE
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  BY THE AMERICAN HAD THE STAME AND AND SET SAND
  SAND SET SAND ASSOCIATED RUSSHOMETER VALYES, F
  TEMPREED GASS SHOWER ENICLOSURE AND DOORTO
  6-07-AGOVE THE DRAIN. TOOR SHALL SWING OUT.
  TEMPREED GASS SHOWER ENICLOSURE AND DOORTO
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  BERLAD, SELLY ALMORAL WIN OF REPRODUCTION OF 
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  MAY BE CONTINUOUS WINDOWS PROPERTY 
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- (N) CONDENSER TO HAVE, A SOUND ATTENUATED CONCRETE & OCK ENCLOSURE TO MEET LAGUNA BEACH EXTERIOR NOBE EQUIPMENTS FOR A RESIDENCE, (7.25.04 EXTERIOR NOBE STANDARDS)
  (7.25.04 EXT

- IN BREC DRIPEWAY
  IN STREET CRIPEWAY
  IN STREET
  IN STREE

- CLERESTORY ALUMINUM WINDOW ROOF MAINTENANCE ACCESS LADDER. 42" HIGH WALL

(N) CONC. REAINING WALL



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Mike and

lohrbach

SECOND FLOOR & MEZZAN NE PLAN

A-2.2

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 10 of 32



#### **General Roof Notes**

ALL RÍDGES, HE'S AND VALEYS SHALL BE FLASHED WITH 24 GA. G.I. METAL FLASHING CONTINUOUS UNDERNEAHT HE AND SHALL NOT BE VERBLE. FLASHING SHALL EXTEND UP AND DOWN ADJACENT SUPERACES, AM, PO IZ "PYPICAL. FLASHING SHALL EXTEND UP AND CONTINUOUS STREY 135" WIPE) OF 309 FEET PAPER. (2) LAYEIS OF #30 FEET PAPER SHALL LAY IN CONTINUOUS STREY OVERALPEN ON HELD.

ALL RIDGES, HPS AND VALLEYS SHALL BE FLASHED WITH 24 GA. G.I. METAL FLASHING CONTRIBUOUS UNDERNEAN HILE AND SHALL NOT BE VISBELE. FLASHING SHALL EXTEND UP AND DOWN ADJACENT SURFACES. AND O' I 2"TYPICAL. FLASHING SHALL BE LED AD ON A CONTRIBUOUS STREY 1.58 WIDE JOY 309 FEET PAPER, 2] LAYERS O' F 830 FEET PAPER SHALL LAY IN CONTRIBUOUS STREY OVERALIZED IN FIELD.

ALL RIDGES, HPS AND VALLEYS SHALL BE FLASHED WITH 24 GA. G.J. METAL FLASHING CONTINUOUS UNDERNEATH TILE AND SHALL NOT BE VISIBLE. FLASHING SHALL EXTEND UP AND DOWN ADJACENT SURFACES A MIN. OF IZ-TYPICAL.

FLASHING SHALL BE LAID ON A CONTINUOUS STRIP ( 36' WIDE) OF 30# FELT PAPER. (2) LAYERS OF #30 FELT PAPER SHALL LAY IN CONTINUOUS STRIPS OVERLAPPED IN FIELD.

ALL RIDGES, HPS AND VALLEYS SHALL BE FLASHED WITH 24 GA. G.I. METAL FLASHING CONTRIBUOUS UNDERNEATH BILE AND SHALL NOT BE VISIBLE. FLASHING SHALL EXTEND UP AND DOWN ADDACENT SUPPLACES. AND OF 12\*TPICAL. FLASHING SHALL BE ALD ON A CONTRIBUOUS STREY 1.56 WIDED OF 30 FEIT PAPER. (2) LAYERS OF #30 FEIT PAPER SHALL LAY IN CONTRIBUOUS STREYS OVERLAPPEN IN FEID.

METAL CHIMNEYS SHALL BE ANCHORED AT EACH FLOOR AND ROOF WITH TWO 1 1/2" BY 1/8" METAL CHYMRETS STATE BE ANGLINEDED I ENCH NOUNE AND ROUTE WITH WO 11/2 B 11/90 M 19/0 M 19/0

#### **Gutters and Drains**

GUTTERS SHALL BE CONSTRUCTED OF PAINTED ALUMINUM WITH 5/8" EXPANSION JOINTS EVERY 30 FFF T MAXIMIM

GUTTER SHALL SLOPE 1/16" PER FOOT TOWARD RAIN WATER LEADERS.

UNLESS SPEC FIED OTHERWISE, RAIN WATER LEADERS ARE EXPOSED AND LOCATION IS SHOWN ON ROOF PLAN.

PROVIDE DOME WIRE BASKET AT EACH RAIN WATER LEADER.

ROOF DRAINAGE TO BE TAKEN TO SPLASH BLOCKS AT GRADE. ALL RAIN WATER SHALL BE D RECTED TO ON-SITE COLLECTION AREA.

#### **Roof Penetrations**

VENTS AND APPLIANCE VENTS SHALL PROJECT ABOVE ROOF BY THE MINIMUM DISTANCE REQUIRED BY APPLICABLE CODES AND SHALL BE LOCATED IN AREAS NOT VEIBLE FROM STREET EXACT LOCATION TO BE COORDINATED WITH ARCHITECT PRIDE TO INSTALLATION.

ALL VEN IS TO HAVE RAIN PROTECTION CAPS.

CONTINUOUS WATERPROOFING AT ALL ROOF PENETRATION SHALL BE PROVIDED, ROUGH CARPEN ITES SHALL PROVIDE 2 X STRPPING ® 16" O.C. AND PLYWOOD. "W.R. GRACE 4000" BITUINENE WEAPPING AND 26 C.G. SHALL BE USED FOR ALL FLASHING AND COUNTERFLASHING. ALL JOINTS AT SHEETMETAL SHALL BE CAULKED.

COLOR OF ALL EXPOSED VENTS AND ROOF STACKS TO MATCH ADJACENT ROOF MATERIAL

ALL FLUES AND VENTS SHALL BE LOCATED IN UNOBTRUSIVE AREAS. RELATIVE TO VIEWS FROM THE STREET AS MUCH AS POSSIBLE.

PROTECTION OF OPENINGS INTO ATTICS, FLOORS OR OTHER ENCLOSED AREAS SHALL BE COVERED WITH CORROSION-RESISTANT METAL MESH WITH MESH OPENINGS OF 1/4" MIN., & 1/2" MAX., IN DIMENSION.

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#### **Roof Plan Keynotes**

CLASS A' ROOF WATER PROOF MEMBRANI
LOW SLOPE ROOF, RUBERCHO
MATERIAL CORP., (ICC-ESP-1274). SEE
ATTACHED DOCUMENT.
ATTACHED DOCUMENT.
BY COLUMENT.
B

FIRE DEPARTMENT SIDE YARD ACCESS
PATHWAY
FIRE DEPARTMENT SIDE YARD ACCESS STAIRS
TO REAR OF BUILDING
HARDWOOD SIDE YARD GATE
DRAINAGE RIDGE 16.



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**ROOF PLAN** A-3.0

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 11 of 32





West Elevation

# North Elevation

#### **Elevation Keynotes**



1. LOW SLOPE ROOF
2. COPPER GUTTER
3. SINGLEY
3. SINGLEY
4. ALLINGHAIN SLONG DOODS
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**ELEVATIONS** NORTH-WEST

A-4.0

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 12 of 32

# MAX. ROOF HT. FROM LOWEST FIN. FLR. B-B A5.0 O. EAVE CEILING HT. 5 SECOND MEZZ, F.F. +68.38 FIRST FLR. F.F.

# South Elevation



East Elevation SCALE: 1/4" = 1'-0"

#### **Elevation Keynotes**



1. LOW SLOPE ROOF
2. COPPER GUTTER
3. SYNTIGHT
3. SYNTIGHT
4. SYNTIGHT
5. ALUMPHUN WINDOWS
6. ALUMPHUN WINDOWS
7. ALUMPHUN WIN



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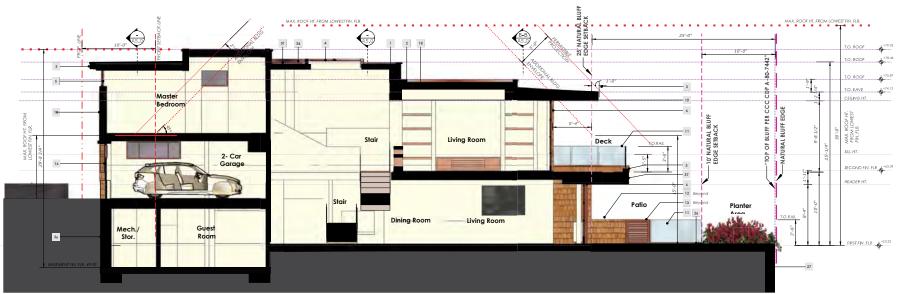
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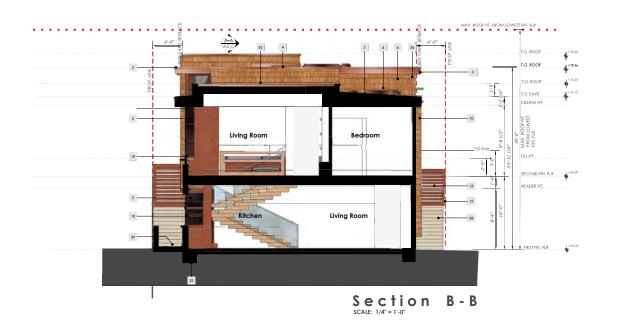
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**ELEVATIONS** SOUTH-EAST A-4.1

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# Section A-A



# lohrbach

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**a** 

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A-A & B-B

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 14 of 32

MATL.
MINIMUM 3 FT. WIDE ALL WEATHER PATH FOR FD
ACCESS AREAS SHALL NOT HAVE A SLOPE EXCEEDING 10%.
AND TO BE OF IMPERVIOUS MATL.

LOW SLOPECIAS W ROOF W/ WATERPROOFING MEMBRANE BY YXXXX SET CLER XXXX, FOR SPECIFICATIONS.

ALMANHAW MODOS

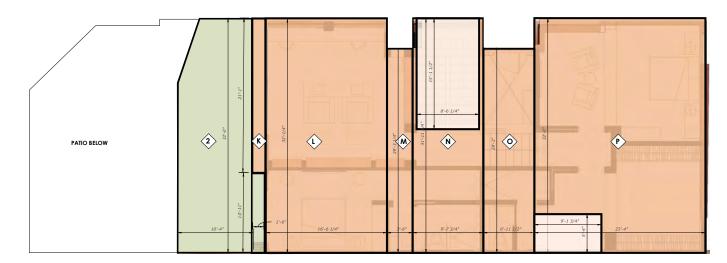
SPECIFICATIONS.

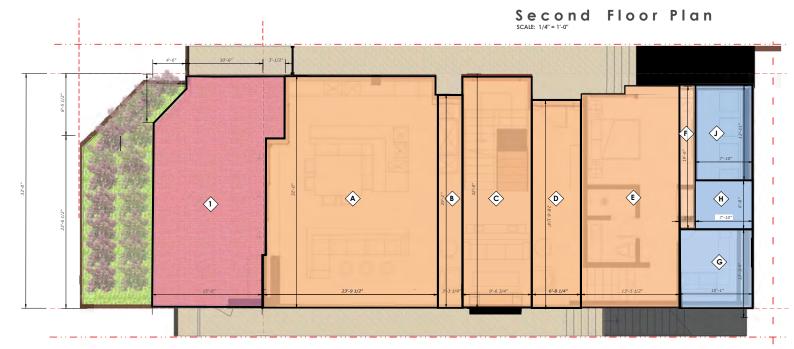
ALMANHAW DOUGH DOOR

SPECIFICATIONS.

SPECIF

**Section Keynotes** 





First Floor Plan

# lohrbach

Milke and Lori Gray Residence 1007 Gaviota Drive Laguna Beach California 92651

ARE	A CALCULATIONS			
$\Diamond$	SYMBOL#			
FIRST FLOOR- BASE. LIVABLE AREA				
Α	761.6 SF			
В	94.3 SF			
С	306.6 SF			
D	190.9 SF			
Е	424.0 SF (BASEMENT)			
F	40.9 SF(BASEMENT)			
TOT	AL LIVABLE AREA 1,818.3 SF			
MEC	H./STORAGE			
G	123.0 SF			

G	123.0 SF			
Н	51.9 SF			
J	100.6 SF			
FIRST	FLOOR PATIO			
1	453.9 SF			
SECOND FLOOR LIVABLE AREA				
K	31.5 SF			
L	528.0 SF			
М	102.4 SF			
N	170.1 SF			
0	203.6 SF			
Р	697.6 SF (MEZZANINE)			
SECO	OND FLOOR DECK			
2	319.3 SF			

TOTA	LE 1,733.2 SF	
CAR	ACE.	
Q	488.8 SF	
TOTAL LIVABLE AREA		3,551.5 SF
TOTAL DECK AREA		319.3 SF



MECH. AREA



Sheet Title:	
	AREA
C	<b>ALCULATIONS</b>

AC-1.0

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California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 15 of 32

# lohrbach

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GARAGE AREA

CARAGE AREA

DECK AREA

= 488.8 SF

Sheel Fille!

AREA

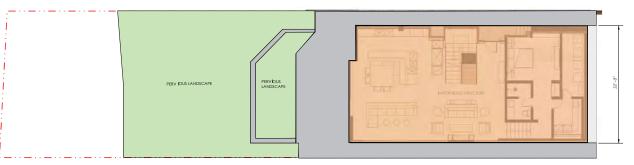
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Garage Floor Plan

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 16 of 32



#### IMPERVIOUS AREA LEGEND

LOT AREA IMPERVIOUS STRUCTURE IMPERVIOUS HARDSCAPE AREA UNDER 3° SIDE 5,181 SF 2,076 SF (40.1%) 914 SF (17.6%) 94 SF (1.8%)

2,990 SF (59.5%) 1,941 SF (40.5%)

TOTAL IMPERVIOUS PERVIOUS LANDSCAPE

PREVIOUS LANDSCAPE IMPERVIOUS LANDSCAPE IMPERVIOUS STRUCTURE AREA UNDER 3' WIDE

OPEN SPACE AREA LEGEND

OPEN SPACE AREA STRUCTURE UNDER ROOF

40% OF GROSS FLOOR AREA = (.4) x 3,551.5 = 1,421 SF OPEN SPACE PROPOSED = 2,739SF = 52.9%

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LOT AREA = 5,181 SF BUILDING AREA = 2,830 SF LOT COVERAGE = 2,830/5,181 = 54.6%

**BUILDING AREA LEGEND** 

LOT AREA

LIVABLE BUILDING AREA BASED ON MUNICIPAL CODE 25.50.004(2).

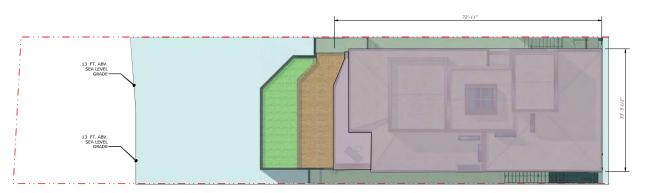
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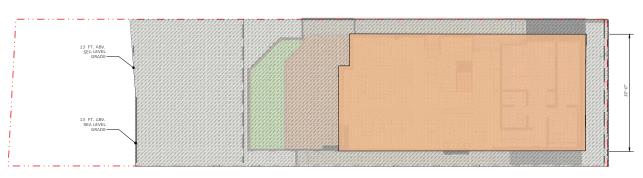
AREA

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 17 of 32

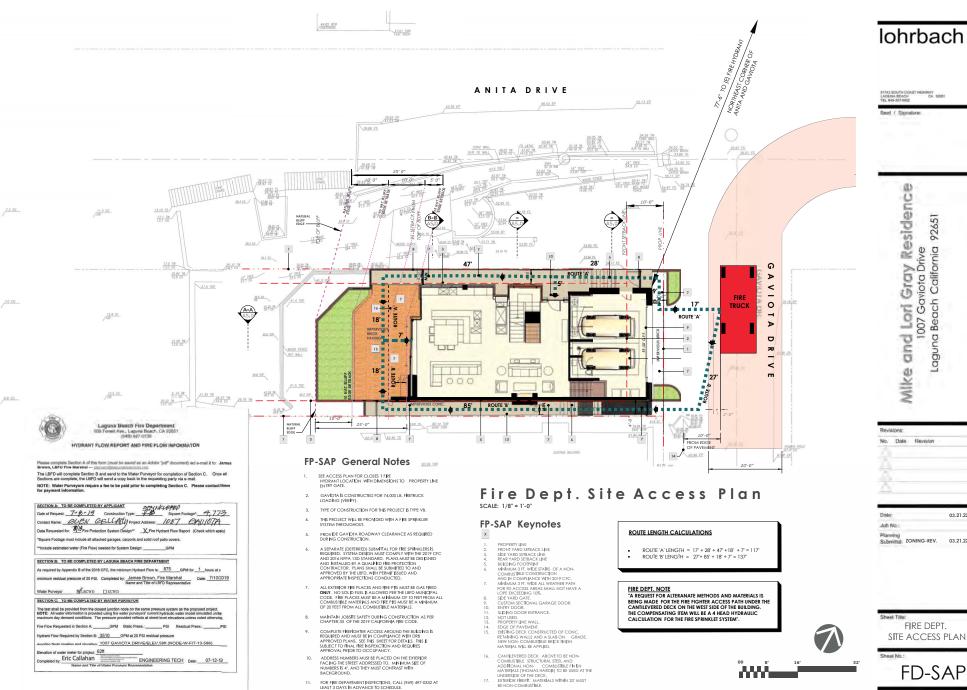
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#### Open Spaced Proposed SCALE: 1/8" = 1'-0"



Lot Coverage Proposed SCALE: 1/8" = 1'-0"



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California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 18 of 32





N-E Perspective - Ex. 2

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### North Perspective Ex. 3



# N-W Perspective Ex. 4

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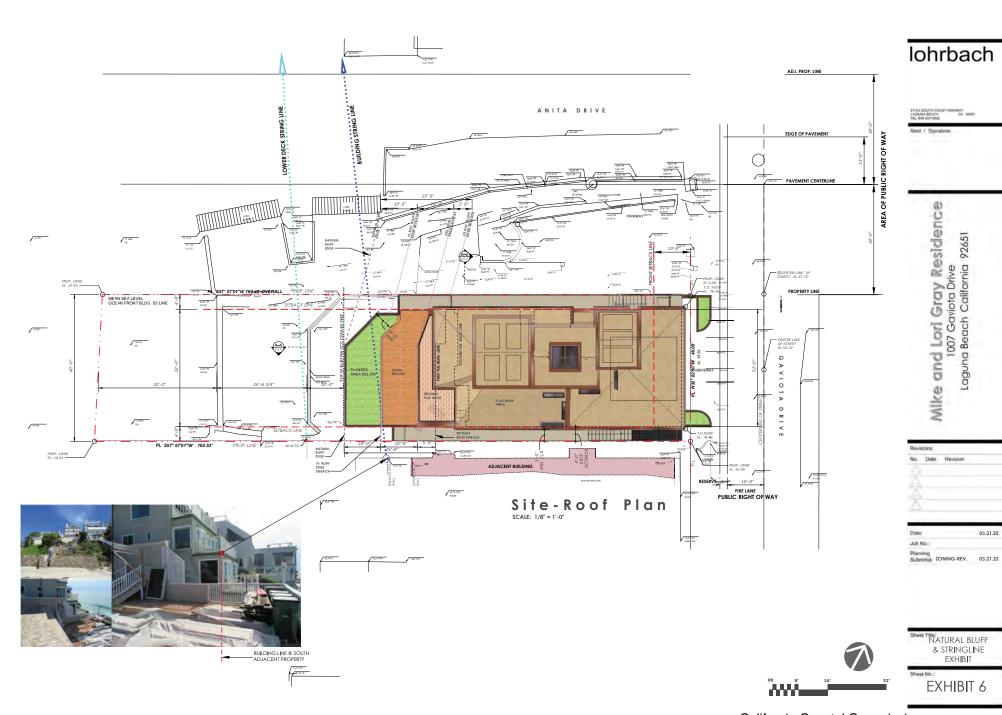
N-W Perspective Ex. 5

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N-W PERSPECTIVE

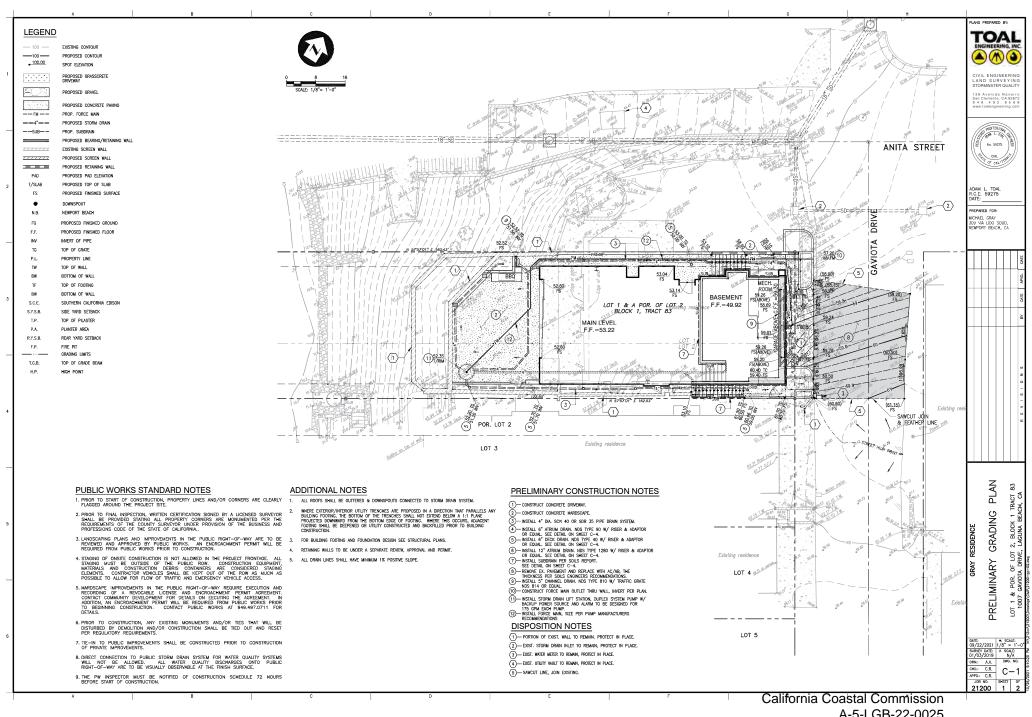
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EXHIBIT 5

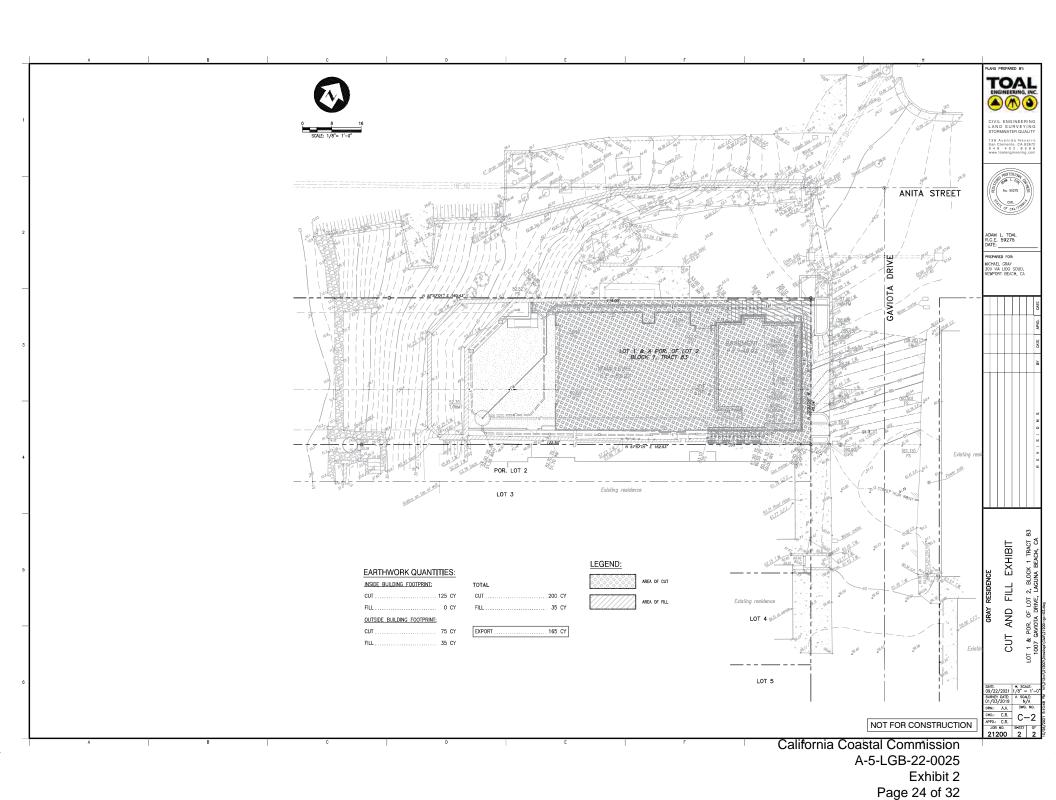
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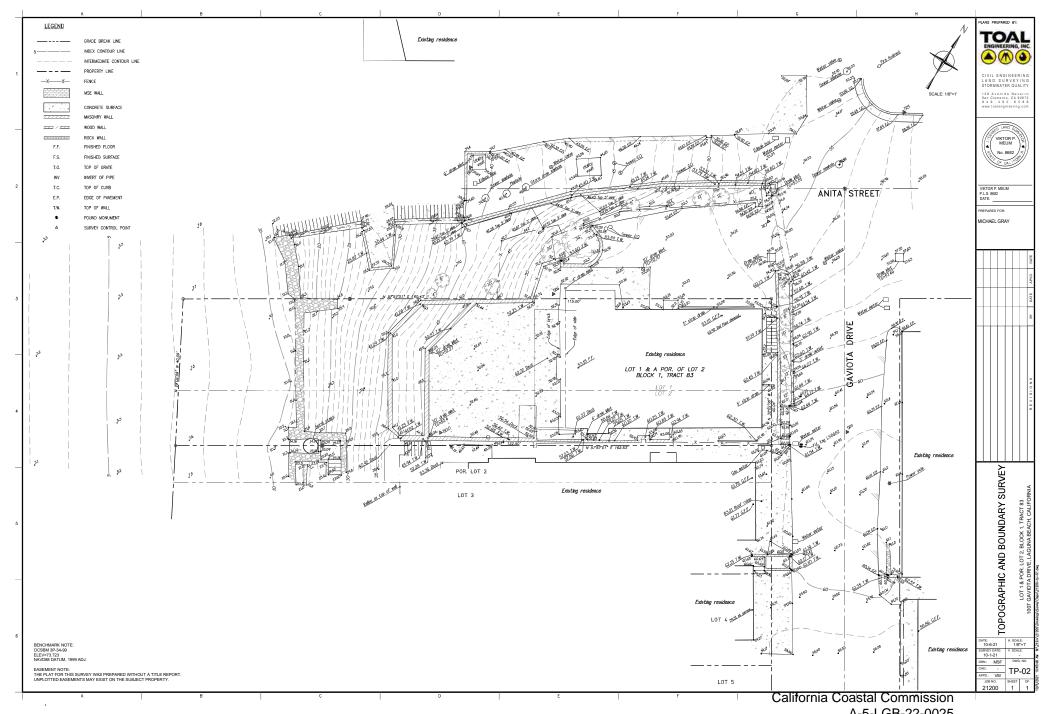


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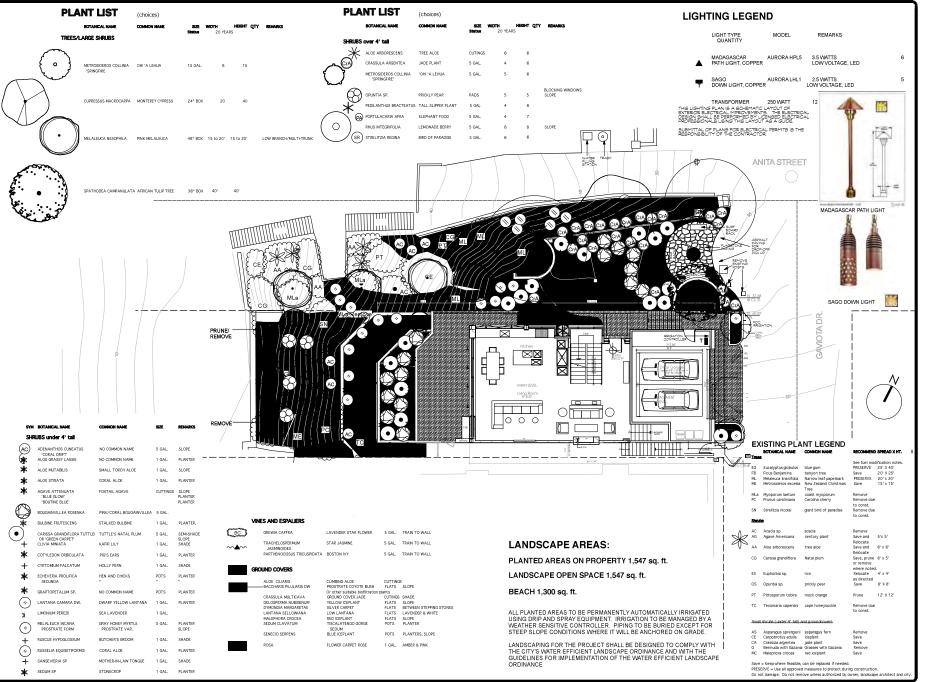


A-5-LGB-22-0025 Exhibit 2 Page 23 of 32





A-5-LGB-22-0025 Exhibit 2 Page 25 of 32



REVISIONS BY 3-9-22 AC

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CLANDSCAFE, ARCHITECT-ASIA
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PRELIMINARY
ANDSCAPE PLAN

GRAY RESIDENCE 1007 GAVIOTA LAGUNA BEACH, CA 92651

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A-5-LGB-22-0025 Exhibit 2 Page 26 of 32

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# Second Floor Plan



#### **Building Exterior Lighting Legend**

SYMBO	OL TYPE	MANUFACTURER	MODEL #	UNITS	WATTAGE	LUMENS
•⊕	EXTERIOR WALL LIGHT	AURORALIGHT	LWM250-C8-GTL CYRANOS	2	3 WATTS (CREE XLAMP LED 2700)	600/UNIT
$\boxtimes$	RECESSED DOWN LIGHT	AURORALIGHT	TAOS: HD11	12	2 WATTS (CREE XLAMP® HIGH INTENSITY (XP-L) LED 2700)	165/UNIT
_	STEP LIGHT	AURORALIGHT	MERIDIAN-LED: LSW8	5	1.25 WATTS (CREE XLAMP® (XP-G) LED 2700)	130/UNIT
	PATHWAY LIGHT	AURORALIGHT	MAGLIO-LED: LMG1-AF	8	2.5 WATTS (CREE XLAMP® (XP-G) LED 2700)	305/UNIT



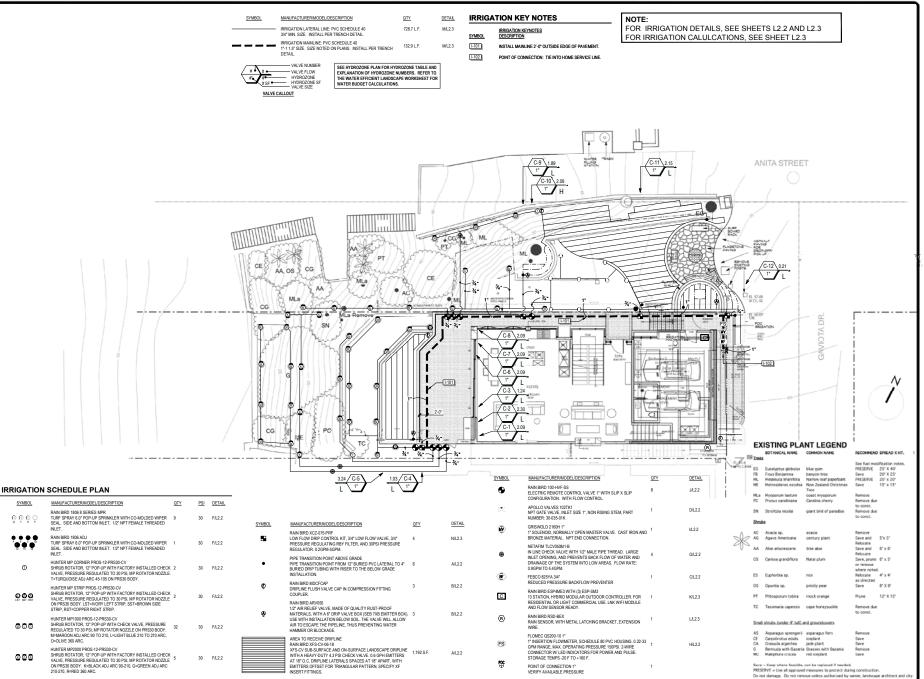
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EXTERIOR BLDG.

LIGHTING

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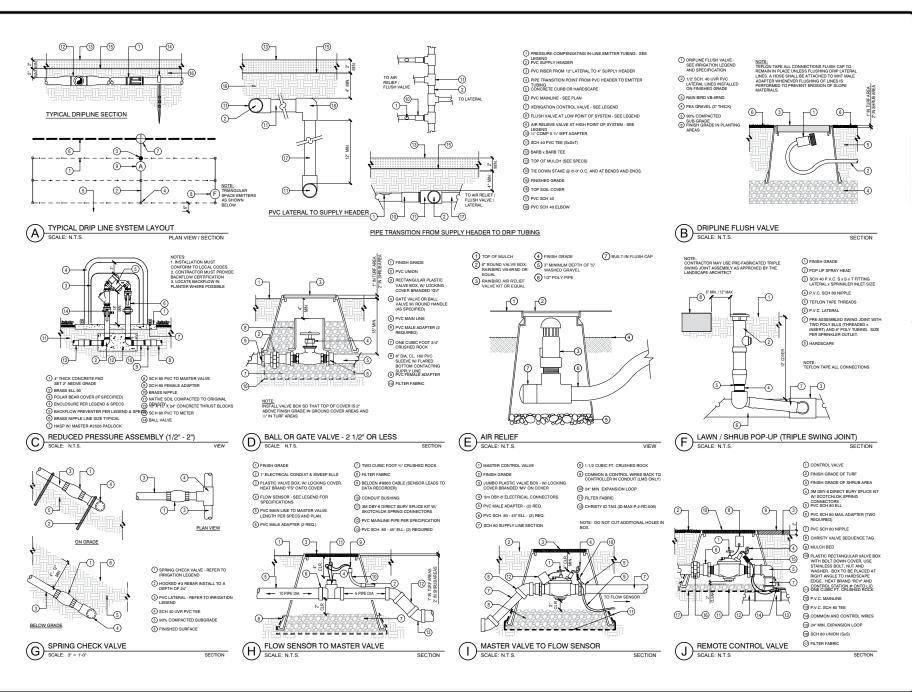
REVISIONS BY

CHRISTOPH CHRIST

RRIGATION PLAN

GRAY RESIDENCE 1007 GAVIOTA LAGUNA BEACH, CA 92651

California Coastal Commission



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IRRIGATION PLAN

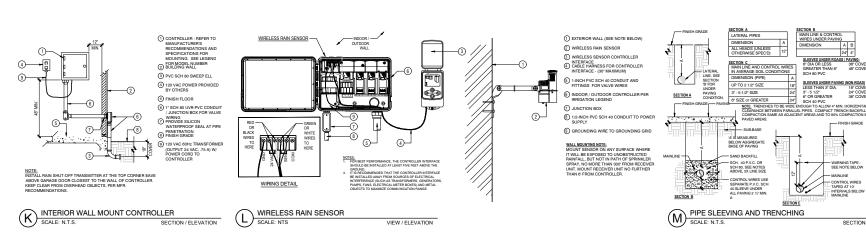
GRAY RESIDENCE 1007 GAVIOTA LAGUNA BEACH, CA 92651

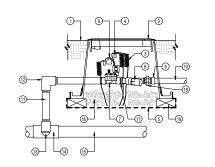




PLAN RIGATION







XERIGATION CONTROL ZONE KIT - LOW FLOW

1 FINISH GRADE / TOP OF MULCH (2) VALVE BOX WITH COVER: JUMBO

SIZE HEAT BRAND 'RCV' AND CONTROLLER STATION # ONTO LID. 3 30-INCH LINEAR LENGTH OF WIRE, COILED

WATERPROOF CONNECTION

(5) FILTER FABRIC

(6) CHRISTY ID TAG (7) REMOTE CONTROL VALVE INCLUDED ON CONTROL ZONE KITI

(INCLUDED ON CONTINUC ZONE
SEE PLAN FOR SIZE.

(a) PRESSURE REGULATING QUICK
FILTER (INCLUDED IN CONTROL
ZONE KIT)

(b) PVC SCH 40 FEMALE ADAPTOR (ii) LATERAL PIPE (TO SYSTEM)

(12) PVC SCH 80 ELL

(3) PVC SCH 80 NIPPLE (2-INCH LENGTH, HIDDEN) AND PVC SCH 80 (14) PVC SCH 80 TEE OR ELL

(15) MAINLINE PIPE

(8) 3-INCH MIN. DEPTH OF 3/4-INCH WASHED GRAVEL

(17) 1" X 3/4" REDUCING COUPLING (B) PVC UNION

(19) BRICK (1 OF 4)

IRRIGATION NOTES:

MAIN LINE PIPING AND CONTROL WIRES UNDER PAVING SHALL BE INSTALLED IN SEPARATE SLEEVES. MAIN LINE SLEEVE SIZE SHALL BE A MINIMUM OF TWICE THE DIAMETER OF THE PIPE TO BE SLEEVED OR AS INDICATED ON THE DRAWINGS. CONTROL WIRE SLEEVES SHALL BE OF SUFFICIENT SIZE FOR THE REQUIRED NUMBER OF WIRES UNDER PAVING

LATERAL LINE PIPING UNDER PAVING SHALL BE PVC SCHEDULE 40 PIPE AND SHALL BE INSTALLED PRIOR TO PAVING.

PIPE SIZES SHALL CONFORM TO THOSE SHOWN ON DRAWINGS. NO SUBSTITUTIONS OF SMALLER PIPE SIZES SHALL BE PERMITTED, BUT SUBSTITUTIONS OF LARGER SIZES MAY BE APPROVED. ALL DAMAGED AND REJECTED PIPE SHALL BE REMOVED FROM THE SITE AT THE SAID TIME OF

FINAL LOCATION OF THE AUTOMATIC CONTROLLER SHALL BE APPROVED BY THE OWNER'S REPRESENTATIVE.

120 V.A.C. ELECTRICAL POWER SOURCE AT CONTROLLER LOCATION SHALL BE PROVIDED BY OTHERS. THE IRRIGATION CONTRACTOR SHALL MAKE THE FINAL CONNECTION FROM THE ELECTRICAL SOURCE TO THE CONTROLLER.

SPRINKLER HEADS SHALL BE PERPENDICULAR TO FINISH GRADE UNLESS OTHERWISE SPECIFIED.

THE IRRIGATION CONTRACTOR SHALL FLUSH AND ADJUST ALL SPRINKLER HEADS AND VALVES FOR OPTIMUM COVERAGE WITH MINIMUM OVERSPRAY ONTO WALKS, STREETS, WALLS, ETC.

THIS DESIGN IS DIAGRAMMATIC. ALL PIPING, VALVES, ETC., SHOWN WITHIN PAVED AREAS IS FOR DESIGN CLARIFICATION ONLY AND SHALL BE INSTALLED IN PLANTING AREAS WHEREVER POSSIBLE. THE CONTRACTOR SHALL LOCATE ALL VALVES IN SHRUB AREAS.

IT IS THE RESPONSIBILITY OF THE IRRIGATION CONTRACTOR TO BECOME FAMILIAR WITH ALL GRADE DIFFERENCES, LOCATION OF WALLS, RETAINING WALLS STRUCTURES AND LITH ITIES. THE IRRIGATION CONTRACTOR SHALL WALLS, STRUCTURES AND DITTIES. THE INTUSTANCE CONTINUED TO STRUCTURE SHALL ALSO COORDINATE WORK WITH OTHER CONTRACTORS FOR THE LOCATION AND INSTALLATION OF PIPE SLEEVES AND LATERALS THROUGH WALLS, UNDER ROADWAYS AND

DO NOT WILLFULLY INSTALL THE SPRINKLER SYSTEM AS SHOWN ON THE DRAWINGS WHEN IT IS OBVIOUS IN THE FIELD THAT UNKNOWN OBSTRUCTIONS, GRADE DIFFERENCES OR DIFFERENCES IN THE AREA DIMENSIONS EXIST THAT MIGHT NOT HAVE BEEN CONSIDERED IN THE ENGINEERING. SLICH OBSTRUCTIONS OR DIFFERENCES SHOULD BE BROUGHT TO THE ATTENTION OF THE OWNER'S AUTHORIZED REPRESENTATIVE. IN THE EVENT THIS NOTIFICATION IS NOT PERFORMED, THE IRRIGATION CONTRACTOR SHALL ASSUME FULL SPRINKLER EQUIPMENT NOT OTHERWISE DETAILED OR SPECIFIED SHALL BE INSTALLED AS PER MANUFACTURER'S RECOMMENDATIONS AND SPECIFICATIONS.

REFER TO SPECIFICATIONS FOR ADDITIONAL DETAILED INFORMATION

ADV (ANTI-DRAIN VALVES) UNITS AS SHOWN IN THE DETAILS ARE FOR TYPICAL INSTALLATION ONLY AND MAY NOT BE REQUIRED ON ALL HEADS. PRIOR TO INSTALLATION THE CONTRACTOR SHALL VERIFY WITH THE ON-SITE GRADES. IF THERE IS AN ELEVATION DIFFERENCE OF 24" OR MORE BETWEEN THE HIGHEST HEAD AND THE LOWEST HEAD ON A SYSTEM, THE ADVS SHALL BE INSTALLED PER THE DETAIL. NO LOW HEAD DRAINAGE ALLOWED

CONTRACTOR TO VERIFY ALL CONDITIONS AND DIMENSIONS SHOWN ON THE PLANS AT THE SITE PRIOR TO COMMENCEMENT WITH ANY WORK UNDER THIS

THE CONTRACTOR SHALL CARRY ALL WORKMAN'S COMPENSATION, PUBLIC LIABILITY AND PROPERTY DAMAGE INSURANCE AS REQUIRED BY THE OWNER.

INSTALL ALL FOLIPMENT AND MATERIALS AS SHOWN ON THE DRAWINGS AND

PRIOR TO COMMENCEMENT OF WORK THE CONTRACTOR SHALL CONTACT THE LANDSCAPE ARCHITECT AND COORDINATE ALL INSPECTIONS

EXTREME CARE SHALL BE EXERCISED IN EXCAVATING AND WORKING NEAR EXISTING UTILITIES. CONTRACTOR SHALL VERIFY THE LOCATION AND CONDITION OF ALL UTILITIES AND BE RESPONSIBLE FOR DAMAGE TO ANY

THE CONTRACTOR SHALL PROTECT WORK FROM DAMAGE AND THEFT AND REPLACE ALL DAMAGED OR STOLEN PARTS AT THEIR EXPENSE UNTIL THE WORK IS ACCEPTED IN WRITING BY THE OWNER.

THIS SYSTEM DESIGN IS BASED ON THE REGULATED OPERATING PRESSURE AND THE MAXIMUM FLOW DEMAND SHOWN ON THE IRRIGATION DRAWINGS AT EACH POINT OF CONNECTION

THE CONTRACTOR SHALL KEEP THE PREMISES CLEAN AND FREE OF EXCESS EQUIPMENT, MATERIALS AND RUBBISH

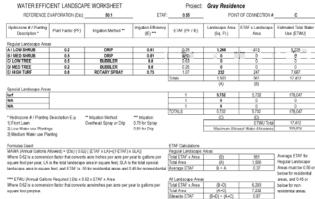
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IRRIGATION WORK SHALL BE GUARANTEED BY THE CONTRACTOR AS TO MATERIAL AND WORKMANSHIP FOR A PERIOD OF ONE YEAR FOLLOWING THE DATE OF FINAL ACCEPTANCE OF THE WORK.

MATERIALS AND EQUIPMENT SHALL CONFORM TO APPLICABLE STATE OF

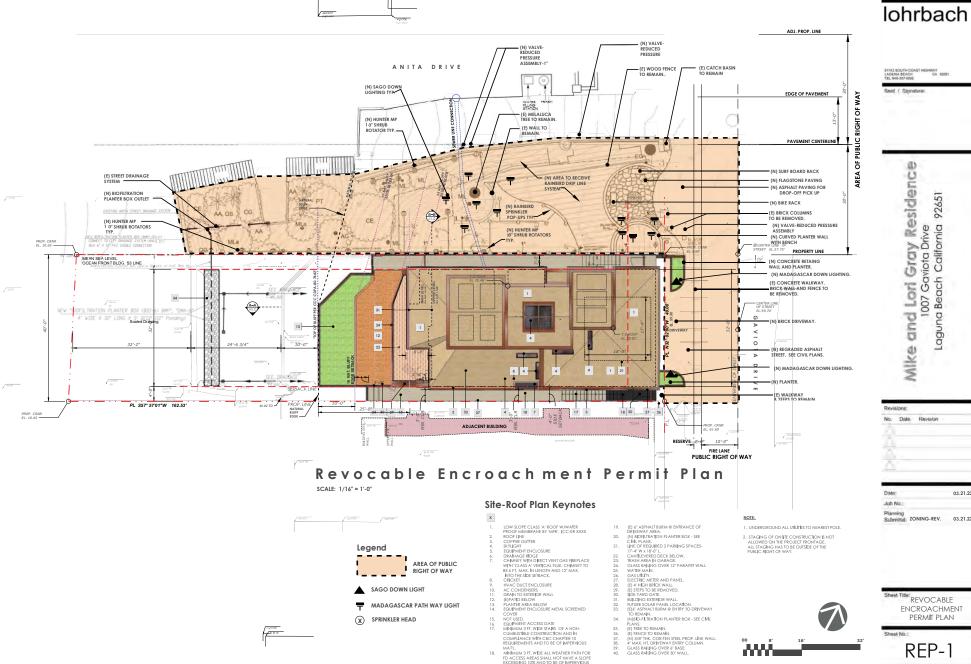


DRIPLINE TOTAL SPRAY TOTAL DRIPLINE



SECTION

California Coastal Commission



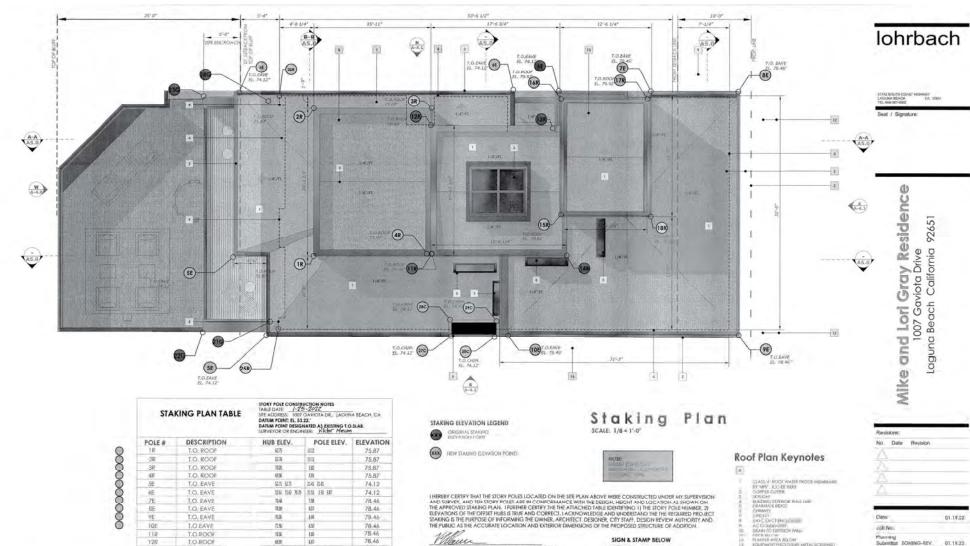
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MATERIAL.

03.21.22 Planning Submittal. ZONING-REV. 03.21.22

Sheet Title: REVOCABLE ENCROACHMENT PERMIT PLAN

REP-1

California Coastal Commission A-5-LGB-22-0025 Exhibit 2 Page 31 of 32



	SIA	KING PLAN TABLE	SITE ADDRESS: 1007 GAVIOTA DR., LAGUNA BEACH, CA DATUM FOINT: EL 53.22. DATUM FOINT DESIGNATED AS EXISTING T.O.SLAB. SURVEYOR OR ENGINEES: VIKIBIT MEUM				
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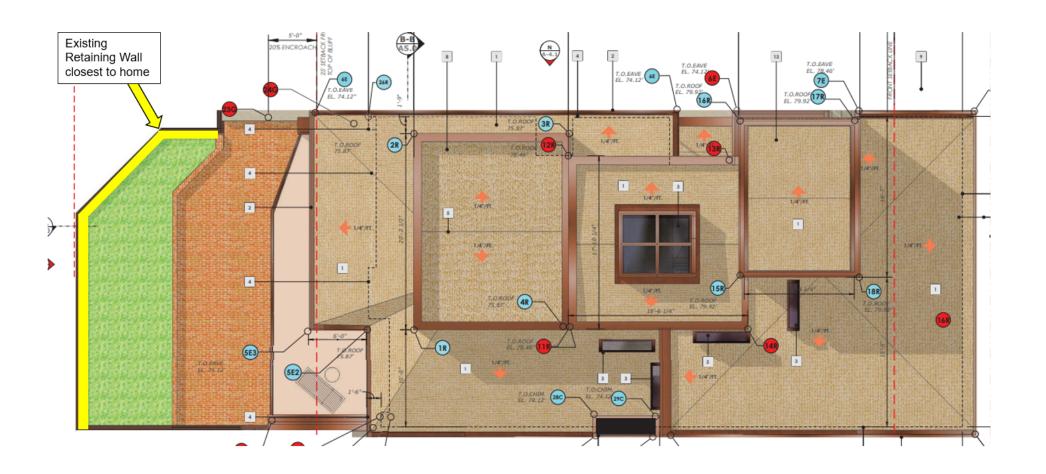


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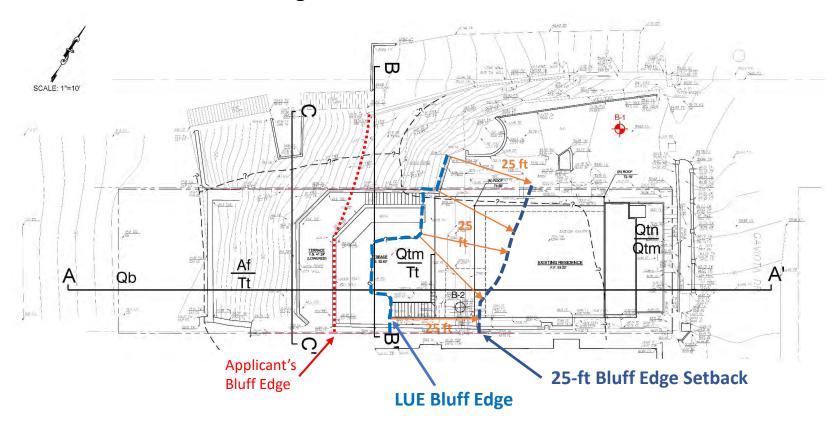
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California Coastal Commission Tolling The 21200 A-5-LGB-22-0025

> Exhibit 2 Page 32 of 32



# **Site Plan with Bluff Edge and Setback Locations**



(modified from Ref. 12)

California Coastal Commission A-5-LGB-22-0025 Exhibit 4 Page 1 of 1

#### CALIFORNIA COASTAL COMMISSION

455 MARKET STREET, SUITE 228 SAN FRANCISCO, CA 94105-2219 VOICE (415) 904-5200 FAX (415) 904-5400



March 30, 2023

#### REVISED BLUFF EDGE & GEOLOGIC REVIEW MEMORANDUM

To: Bailey Warren, Coastal Program Analyst

From: Joseph Street, Ph.D., P.G., Staff Geologist

Re: 1007 Gaviota Dr., Laguna Beach (Gray Residence)

Appeal No. A-5-LGB-22-0025

This memorandum is an update to the review memo included as Exhibit 5 to the previously published staff recommendation on this appeal, both dated February 24, 2023. The current memo reviews new information provided by the applicant and recovered from City and Commission records, and revises several of the conclusions reached in my earlier review. However, my recommendation as to the location of the bluff edge remains unchanged.

The purpose of this memorandum is to (a) determine the position of the bluff edge, consistent with the City of Laguna Beach Local Coastal Program (LCP) definition, on the subject property; and (b) evaluate the bluff top setback necessary to ensure the stability of the new development over its economic life without reliance on shoreline protection. To this end, I have reviewed the following documents provided by the applicant or otherwise directly addressing conditions on the site:

- 1) Geofirm, Inc. and E. J. Miller, Inc., 1980, "Limited Geotechnical Investigation, Slope Instability and Remedial Design Recommendations, 1021 and 1031 Gaviota Street, Laguna Beach, California", May 30, 1980, signed by H. Lawrence and E. J. Miller.
- 2) E. J. Miller, Inc., 1980, "Proposed Design Scheme for Stabilizing the Failed Slope on the Seaward Side of the Residence at 1007 Gaviota Drive, Laguna Beach, California", October 23, 1980, signed by E. J. Miller.
- 3) E. J. Miller, Inc., 1981, "Final Report of Observations and Tests during Repair of the Slope on the Seaward Side of the Residence at 1007 Gaviota Drive, Laguna Beach, California", May 19, 1981, signed by E. J. Miller.
- 4) Geofirm, Inc., 2015, "Geotechnical Bluff Top Evaluation, 1007 Gaviota Dr., Laguna Beach, California", May 8, 2015, signed by H. H. Richter and K. A. Trigg.
- 5) Geofirm, Inc., 2016, "Preliminary Geotechnical Investigation For Residence Remodel and Additions, 1007 Gaviota Dr., Laguna Beach, California", July 20, 2016, signed by E. Hilde and E. J. Aldrich.
- 6) Geofirm, Inc., 2019a, "Geotechnical Slope Stability Determination, 1007 Gaviota Dr., Laguna Beach, California", April 8, 2019, signed by Z. Wang and K. A. Trigg.

- 7) Geofirm, Inc., 2019b, "Updated Preliminary Geotechnical Investigation For Residence Remodel and Additions and Response to Review Dated June 17, 2019, 1007 Gaviota Dr., Laguna Beach, California", July 16, 2019, signed by K. A. Trigg and Z. Wang.
- 8) Geofirm, Inc., 2019c, "Clarification of Bluff Edge Determination, 1007 Gaviota Dr., Laguna Beach, California", September 18, 2019, signed by K. A. Trigg.
- 9) GeoSoils, Inc., 2021, "Discussion of Coastal Hazards and Wave Runup, 1007 Gaviota Drive, City of Laguna Beach, Orange County, California", October 8, 2021, signed by D. W. Skelly.
- 10) Geofirm, Inc., 2021, "Review of Slope Retaining Walls and Bluff Edge Determination, 1007 Gaviota Dr., Laguna Beach, California", October 22, 2021, signed by K. A. Trigg.
- 11) GeoSoils, Inc., 2022, "Final Coastal Bluff Edge Evaluation, 1007 Gaviota Drive, Laguna Beach, Orange County, California 92651", dated February 22, 2022, signed by J. P. Franklin and D. W. Skelly.
- 12) Stoney Miller and Geofirm Consultants, Inc., 2022, "Review of Revised Residence Plans and Slope Stability, Response to Coastal Commission Comments, 1007 Gaviota Dr., Laguna Beach, California", October 3, 2022, signed by K. A. Trigg and H. H. Richter.
- 13) Stoney Miller and Geofirm Consultants, Inc., 2023, "Response to Coastal Commission Email dated January 4, 2023, 1007 Gaviota Dr., Laguna Beach, California", January 13, 2023, signed by K. A. Trigg.
- 14) Stoney Miller and Geofirm Consultants, Inc., 2023, "Response to Bluff Edge & Geologic Setback Review Memorandum dated February 24, 2023, Exhibit 5 to De Novo Appeal A-5-LGB-22-0025, 1007 Gaviota Drive, Laguna Beach, California", dated March 3, 2023, signed by K. A. Trigg.

I have also consulted oblique aerial photographs of the site provided by the California Coastal Records Project (<a href="https://www.californiacoastline.org">https://www.californiacoastline.org</a>) and historical overhead aerial photographs of the site from the University of California Santa Barbara Library archive (<a href="https://mil.library.ucsb.edu/ap\_indexes/FrameFinder/">https://mil.library.ucsb.edu/ap\_indexes/FrameFinder/</a>, accessed January 27, 2023). I have also viewed the bluff and project site from the beach on several occasions, most recently on February 18, 2020.

### **Site Description**

As described in the geotechnical investigations provided by Geofirm (Refs. 5, 7), the coastal bluff at the site is composed of Topanga Formation siltstone and sandstone bedrock overlain unconformably by geologically recent, sandy marine and non-marine terrace deposits. The exterior face of the bluff is largely composed of artificial fill supported by a masonry wall at the bluff toe and two upper bluff retaining walls (Figs. 1, 2). The stabilization system also includes a zone of buried concrete that provides a footing for the upper retaining walls. The fill slope and retaining wall system was constructed in 1980-81 (under Coastal Development Permit No. A-80-7442), in response to bluff erosion and instability affecting both the 1007 Gaviota Dr. property and the neighboring lot to the south (1021 Gaviota Dr.). Ref. 1 described landslides underlying the westernmost portion of the 1007 Gaviota Dr. property, the sewer lift station at the end of Anita St. (neighboring site to the north) the bluff seaward of 1021 Gaviota Dr.:

The landslides involve the movement of bedrock downslope along bedding in clay-rich shale strata which has an out-of-slope dip component. Movement has been triggered primarily by removal of downslope stratigraphic support due to general seacliff retreat. Failure of the bedrock promoted concomitant slumping of upslope terrace deposits. Such failure was

probably also promoted by high groundwater pore pressures resulting from the infiltration of dispersed precipitation upon the slope and general region coupled with concentrated discharge from the deck area ...

Ref. 14 indicates that the landslides occurred during the rainy winter of 1980. Refs. 5 and 7 suggest that some previous sliding and bluff erosion may have been triggered by heavy rains during the winter of 1969.

Based the information contained in the Geofirm reports (Refs. 1, 4, 7, 8), the subject site extends from an elevation of approximately 10 feet above mean sea level (MSL) at the back of the beach to about +60 feet MSL at Gaviota Dr. (Figs. 1, 2). The edge of the rearyard patio (i.e., the top of the uppermost retaining wall and edge of the fill slope) occurs at an elevation of about +52 feet MSL, and the geologic reports (e.g., Refs. 5, 7, 13, 14) indicate that the natural marine terrace deposits behind the fill also extend to this elevation. In its current state, including the fill and retaining walls, the bluff (along Section A-A', Fig. 2) has an average slope of about 48 degrees (or about 1:1 horizontal to vertical, h:v). Cross-sections in Refs. 1, 5 and 7 indicate that the natural bluff beneath may have an average slope of 40 – 42 degrees, but with steeper sections of 65 – 80 degrees.

#### **Coastal Bluff Edge Determination**

The Land Use Element (LUE) of the City of Laguna Beach's certified Local Coastal Program includes the following definition of "Oceanfront Bluff Edge or Coastal Bluff Edge" (Glossary Definition 101) [emphasis added]:

The California Coastal Act and Regulations define the oceanfront bluff edge as the upper termination of a bluff, cliff or seacliff. In cases where the top edge of the bluff is rounded away from the face of the bluff, the bluff edge shall be defined as that point nearest the bluff face beyond which a downward gradient is maintained continuously to the base of the bluff. In a case where there is a step like feature at the top of the bluff, the landward edge of the topmost riser shall be considered the bluff edge. Bluff edges typically retreat over time because of erosional processes, landslides, development of gullies, or by grading (cut). In areas where fill has been placed near or over the bluff edge, the original bluff edge, even if buried beneath fill, shall be taken to be the bluff edge.

This definition is similar, though not identical to the definition of "bluff edge" contained in the Coastal Commission's regulations (Cal. Code Reg. Title 14, §13577(h)).¹ Notably, the LUE definition specifies that grading cuts act as an erosional process that cause the bluff edge to retreat, while artificial fill placed near or over the bluff edge is to be discounted and the edge of the buried natural bluff materials used as the bluff edge. The LUE (in Definition 102) further clarifies that a coastal bluff encompasses the entire slope between the upland area and the beach, and not just the steepest portion of the slope:

Oceanfront Bluff/Coastal Bluff – A bluff overlooking a beach or shoreline or that is subject to marine erosion. Many oceanfront bluffs consist of a gently sloping upper bluff and a steeper lower bluff or sea cliff. The term "oceanfront bluff" or "coastal bluff" refers to the entire

<sup>&</sup>lt;sup>1</sup> Section 13577(h)(2) of the Commission's regulations defines the "bluff edge" as follows:

Bluff line or edge shall be defined as the upper termination of a bluff, cliff or seacliff. In cases where the top edge of the cliff is rounded away from the face of the cliff as a result of erosional processes related to the presence of the steep cliff face, the bluff line or edge shall be defined as that point nearest the cliff beyond which the downward gradient of the surfaces increases more or less continuously until it reaches the general gradient of the cliff. In a case where there is a steplike feature at the top of the cliff face, the landward edge of the topmost rise shall be taken as the cliff edge.

slope between a marine terrace or upland area and the sea. The term "sea cliff" refers to the lower, near vertical portion of an oceanfront bluff. <sup>2</sup>

At the project site, a bluff edge determination pursuant to the LUE definition must take into consideration both the grading cuts and placement of fill on the bluff associated with the 1980-81 slope repairs and wall installation, which first modified and then obscured the bluff edge.

The applicant's earlier bluff edge evaluations (see Refs. 4, 5, 7, 8, 10) posed two basic arguments. The first was that seaward facing slope at the site does not constitute a coastal or oceanfront bluff under the LCP because the average slope of the natural (prestabilization) bluff is less than 45 degrees, and thus does not meet the threshold in the Municipal Code definition (Sec. 25.50.004(a)). This argument is incorrect for several reasons. First, while I agree that the average slope of the natural bluff face, behind the fill and retaining walls, is slightly less than 45 degrees, it also appears to have multiple steeper sections with slopes exceeding 45 degrees. Thus, the bluff here would appear to be a bluff with irregular slope or "multiple slope condition" under Section 25.50.004(a)(i), with a bluff edge at the "most inland 45 degree or greater slope", which at the subject site occurs at the upper edge of the marine terrace deposits at an elevation of approximately 52 feet MSL. Second, and more importantly, the coastal bluff and bluff edge definitions in the LUE, which are determinative in this case, contain no slope-based restrictions on what qualifies as an "oceanfront bluff". The seaward facing slope at this site qualifies as a coastal bluff under the LCP.

The second argument presented, that the Commission has already delineated the bluff edge as the top of the uppermost retaining wall approved under the 1980 CDP, is non-technical in nature and is addressed in the staff report (see section C, Coastal Hazards).

In a later applicant submittal, the GeoSoils "Final Coastal Bluff Edge Evaluation" (Ref. 11), the coastal bluff edge as it existed historically, prior to the 1980-81 stabilization work, was evaluated using stereoscopic analysis of overhead aerial photographs dating from 1947 and 1963. GeoSoils reported that the position of the bluff edge did not change between these two dates, and that the historical bluff edge line was coincident with the top of the uppermost retaining wall across much of the subject site (Fig. 1). This is a useful study, as it provides an estimate of the bluff edge position prior to both the 1980 landslide and the grading cuts and fill placement associated with the construction of the retaining walls. However, the applicant's bluff edge line does not represent the bluff edge under the LUE definition because it does not account for the bluff edge retreat that resulted from grading cuts during the upper retaining wall construction in 1980-81 (described in Refs. 3 and 14).

However, the Municipal Code definitions predate the certification of the 2012 Land Use Element, and the Commission has through numerous prior actions found that the LUE coastal bluff and bluff edge definitions supersede the older definitions in cases where they conflict.

California Coastal Commission A-5-LGB-22-0025 Exhibit 5 Page 4 of 10

<sup>&</sup>lt;sup>2</sup> The Laguna Beach Municipal Code Section 25.50.004 contains a somewhat different definition of a coastal/oceanfront bluff and coastal bluff edge:

<sup>(</sup>a) An "oceanfront bluff" is an oceanfront landform having a slope of forty-five degrees or greater from horizontal whose top is ten or more feet above mean sea level.

<sup>(</sup>i) In cases where an oceanfront bluff possesses an irregular or multiple slope condition, the setback will be taken from the most inland forty-five degree or greater slope.

<sup>(</sup>ii) In cases where the landform constitutes an oceanfront bluff whose slope is less than forty-five degrees, a determination as to whether or not the specific landform is subject to this provision shall be made by the director of community development.

Rather, Ref. 11 posits a bluff edge line that longer existed (or had been substantially altered) by the time walls were constructed.

The construction of the existing retaining wall system at 1007 and 1021 Gaviota Dr. required significant excavation and grading on the bluff face to install the wall footings (Refs. 3, 14). At the top of the bluff, the installation of the upper wall involved a significant cut (8-10 feet wide, up to 12-14 feet deep) into the native upper bluff materials. This cut removed the pre-existing bluff edge, and along the central portion of the site (section A-A', Fig. 2), retreated the bluff edge (the top edge of the natural marine terrace deposits) approximately 10 feet landward. Once the wall and footings were installed, the cut was backfilled with sandy fill.

Ref. 14 notes that the cuts associated with the wall installation were temporary, lasting only as long as the construction effort, and were backfilled to restore the bluff to near its former position. While recognizing the validity of these statements, I do not see that they change the bluff edge delineation under the LUE definition. The LUE definition explicitly recognizes that "[b]luff edges typically retreat over time because of erosional processes, landslides, development of gullies, or by grading (cut)", and does not make a distinction between situations in which a cut is backfilled or left open. To the contrary, the LUE definition provides specific direction that fill be discounted when delineating the bluff edge. In the present context, the most logical interpretation of the phrase "original bluff edge" cited in the definition is the bluff edge as it existed immediately prior to the fill placement, i.e., the edge of recently cut natural upper bluff materials. Otherwise, the phrase "original bluff edge" could be taken to mean the bluff edge at any arbitrary past point in time.

With these considerations in mind, the coastal bluff edge on the subject lot, as defined in the LUE, occurs at the seaward edge of the natural marine terrace deposits where they contact the artificial fill. This is the remnant edge of the cut described in Ref. 3. Along cross-section A-A', across the central portion of lot, the LUE bluff edge occurs about 10 feet landward of the top of the upper retaining wall (i.e., the seaward edge of the fill), at an elevation of about +52 feet MSL (Fig. 2). Geofirm (Refs. 5, 7, 13, 14) has traced the location of this geologic contact (between fill, "Af", and upper bluff marine and non-marine terrace deposits, "Qtm" and "Qtn", respectively) across the site in its plan view figures (see Fig. 1). Along the northwestern flank of the site, on the lot immediately upcoast, the contact between the fill and non-marine terrace deposits appears to curve seaward (downslope), such that the upper portion of the bluff consists of natural terrace deposits rather than fill. In this area, the bluff edge is taken to be the top of the slope, approximately following the +53 ft MSL contour (Fig. 1).

### **Bluff Top Setback**

The City of Laguna Beach LCP requires new principal development to be set back a minimum of 25 feet from the coastal bluff edge (LUE Action 10.2.7), with additional provisions that the setback be increased as necessary to address coastal hazards. Specifically, LUE Action 10.2.6 requires the setback be "a sufficient distance to ensure stability, ensure that it will not be endangered by erosion, and to avoid the need for protective devices during the economic life of the structure (75 years)." The policy further specifies that the development must *maintain* a minimum factor of safety against landsliding of 1.5 (static) or 1.2 (pseudostatic) over this timeframe, taking into account future bluff retreat and, among other things, the effects of sea level rise. In order to

conform to this policy, it is necessary to estimate a safe setback distance without relying on existing or future protective devices, including the existing retaining walls.

### **Bluff Stability**

As noted above, the project site has experienced landsliding and bluff instability in the past, likely occurring along inclined strata in the Topanga Formation bedrock and triggered by (i) marine erosion at the bluff toe over time and (ii) saturation of upper bluff materials during winter storms (Refs. 1, 5, 7, 14). Without the protection and support provided by the existing wall system, similar bluff erosion and instability would be likely to recur in the future. The applicant's initial slope stability analyses (Refs. 5 - 7), relying on relatively conservative assumptions about the shear strengths of the bluff materials (and the bedrock strata in particular), indicated the need for a large setback (about 59 feet from the top of the upper retaining wall) in order to achieve a 1.5 (static) factor of safety; based on this analysis, use of a lateral stability caisson array was recommended to increase bluff stability and allow for the proposed redevelopment, which at that point involved a larger, more seaward-located structure. Ref. 12, submitted in support of the current project proposal, included a revised slope stability analysis using a higher along-bedding shear strength value for the Topanga Formation strata. This revision was based on newly recovered, site-specific information contained in the engineering design reports for the existing retaining wall system (Ref. 3). The revised analysis indicated that, in the absence of the retaining wall system, a 1.5 factor of safety against landsliding was achieved approximately 14 feet landward of the top of the uppermost retaining wall (Section A-A').

The use of greater along-bedding shear strength values for the Topanga Formation rock appears to be justified by prior data, indicating that the revised slope stability analysis is valid. However, it is worth noting that though the retaining wall system was excluded from the analysis, the buried concrete fill that provides foundation support for the walls was not, and thus the analysis may not represent a completely "unprotected" bluff condition. This concrete fill is integrated into the existing bluff face and could not be removed without significant excavation and damage to the natural bluff, and in my view the revised analysis in Ref. 12 provides a reasonably realistic snapshot of bluff stability if the primary protective structures – the exterior walls -- were absent.

#### **Bluff Retreat**

Assessing the amount of future bluff erosion and retreat that could occur at the project site in the absence of the shoreline protection is complicated by the fact that the existing wall system has been in place for the last 40 years, and has effectively halted natural erosion processes at the site over that time period. As a result there is only limited historical information, and no recent evidence, on which to base future retreat estimates. The applicant's coastal hazards analysis (Ref. 9) does not address this issue directly, simply noting that there is little visual evidence of bedrock or upper bluff erosion or beach narrowing in the area in a comparison of recent (March 2020) and historical (February 1963) aerial photographs, and estimating an erosion rate of 0 ft/yr. over this period. Ref. 9 does not discuss the prior landsliding at the site or the large amount of fill that was placed on the bluff during the 1980-81 stabilization work, which would have obscured any visual evidence of bluff erosion that occurred between 1963 – 1980 (Refs. 1, 5, 7, 14). Ref. 9 also makes no allowance for the possibility that future sea level rise could increase bluff erosion at the site.

The geologic reports by Geofirm provide more information about historical bluff erosion at the site, generally concluding that past erosion episodes have been relatively minor. Past rates of erosion and retreat at the bluff toe, pre-dating the lower seawall, appear to have been low, consistent with the relatively resistant nature of the Topanga Formation bedrock. Ref. 1 reports a bedrock erosion rate of 0.5 – 1 inch/year (0.04 – 0.08 ft/yr.) from a prior study. Ref. 7, based on examination of historical aerial photographs dating to 1931, finds no evidence of bluff toe erosion but indicates that some upper bluff erosion may have occurred between 1964 and 1970:

In addition, the yard area backing the residence appears significantly reduced on the seaward edge in the images from 1970. It appears some material was lost at the top, possibly following the winter of 1969. The 1970 toe of the slope appears to be in the same location as 1931 and 1964, suggesting the material loss is not associated with a gross failure. It is our interpretation the upper portion of the slope, possibly within the terrace sand, failed after increased saturation and flowed along the terrace bedrock contact following the heavy rainfall season.

However, the amount of bluff edge retreat thought to have occurred in 1969 was not quantified. As noted above, additional landsliding occurred at the site during the rainy winter of 1980 and provided the impetus for the construction the existing retaining wall system (Refs. 1-3, 14). However, cross-sections of the 1007 and 1021 Gaviota sites attached to Ref. 1 (newly recovered from Commission files) indicate that the landsliding was more severe on the 1021 Gaviota lot, and that bluff erosion at the 1007 Gaviota site was confined to the bluff face, with little or no retreat of the bluff edge. As described above, most or all of the bluff edge retreat that occurred in 1980-81 was due to grading cuts during the installation of the upper wall rather than natural erosion.

The available evidence suggests that significant bluff erosion at the site occurred only infrequently in the past, typically in conjunction with extreme rainfall events, but does not provide a strong basis for estimating future bluff retreat over the next 75 years. This is particularly true due to the potential for significant sea level rise over this period. By driving shoreline retreat, narrowing beaches, and increasing the frequency and energy of wave attack at the base of coastal bluffs, sea level rise is expected to increase rates of bluff erosion. Relying on historical observations alone risks underestimating future bluff retreat. The applicant's coastal hazards report (Ref. 9) discounts the potential for sea level rise to increase bluff erosion at the site. Nonetheless, the wave runup analysis contained in this study does indicate that storm waves can reach and overtop the lower seawall, and would reach progressively higher elevations on the bluff face in the future with sea level rise (SLR). Particularly in the absence of armoring, this would be expected to trigger new episodes of bluff erosion, potentially at rates higher than observed historically.

In order to get a rough sense of how much bluff retreat could occur at the site in the future, I have consulted the USGS CoSMoS bluff retreat tool (Barnard et al. 2018), which includes bluff retreat projections for several transects in the immediate project area, for several different sea level rise scenarios. The direct CoSMoS projections are less useful in the Laguna Beach area because one of the key model inputs, the historical bluff retreat rate, tends to be inaccurate due to the low resolution of the historical maps used in estimating these rates. To partially circumvent this weakness, I have instead (a) used the CoSMoS projections to calculate the factor by which bluff retreat is projected to increase, above the initial rate, for a given amount of SLR (in 2100), and (b) applied this factor to several estimates of the historical bluff retreat rate to generate future bluff retreat projections for several SLR scenarios. For the historical bluff retreat rate, I used the range cited by Ref. 1

(0.04 - 0.08 ft/yr.), along with an average rate (0.24 ft/yr.) provided by USGS for the four CoSMoS transects nearest the project site. For SLR scenarios of 1 - 2 m (3.3 - 6.6 ft) by 2100, CoSMoS projects that average bluff erosion rates (for the period 2016 – 2100) in the project vicinity could increase by factors of 1.3 - 2 (130 - 200%) above the historical baseline. Applied to the historical retreat rates from Ref. 1, these factors of increase in the rate of bluff erosion would result in 4 - 16 feet of bluff retreat over the next 75 years. Using the higher USGS historical retreat rate, the projections increase to 23 - 48 ft over the next 75 years.

#### **Total Setback (No Armoring Condition)**

Combined with the 14-foot setback needed to assure a 1.5 (static) factor of safety under present day conditions, the above bluff retreat projections suggest the need for a total geologic setback on the order of 18 – 30 feet (for the more realistic historical bluff retreat rates from Ref. 1) or 37 – 62 feet (for the higher USGS retreat rates), without relying on shoreline protection. Based on the relatively resistant bedrock present at the bluff toe, and the low frequency of significant bluff erosion episodes observed in the decades prior to 1980, I suspect that the lower bluff retreat projections are more realistic, even for the relatively high sea level rise scenarios examined in my rough analysis. Nonetheless, the large range in the bluff retreat projections underscores the high level of uncertainty in predicting the bluff erosion response to future conditions.

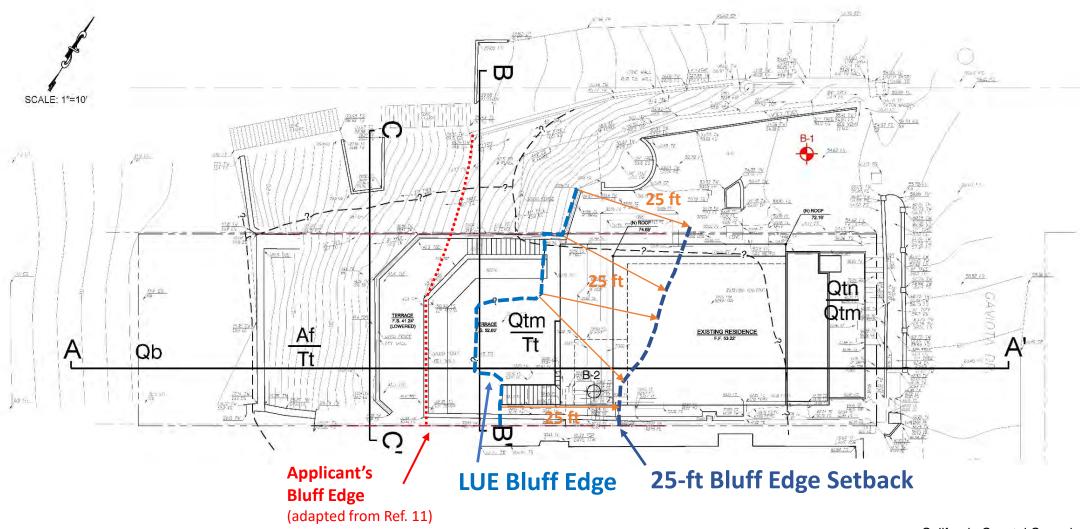
The City LCP requires a minimum 25-foot development setback from the bluff edge for new principal development. As shown in Fig. 1, a 25-ft setback from the LUE bluff edge, would result in larger setbacks – on the order of 40 – 50 feet from the top of the existing fill slope (i.e., top of the upper retaining wall), which extends seaward of the natural bluff face, across most of the subject lot. The 40 – 50-foot geologic setbacks that would result from applying the default 25-foot *bluff edge* setback³ would provide a substantial buffer against future increases in the bluff erosion rate due to SLR. For these reasons, I believe that a development setback of 25 feet from the coastal bluff edge, as defined in the City's certified LUE and illustrated in Fig. 1, is likely to ensure the safety and stability of new development at the site over a 75-year economic life, without reliance on shoreline protection. However, given the uncertainties involved, it would still be prudent to include special conditions to further minimize hazards, such as a deed restriction and assumption of risk provision to make the permittee and future owners aware of the hazards inherent to this location, and a requirement that the new development be removed or relocated if it is threatened by erosion in the future.

Attachments: Figures 1, 2

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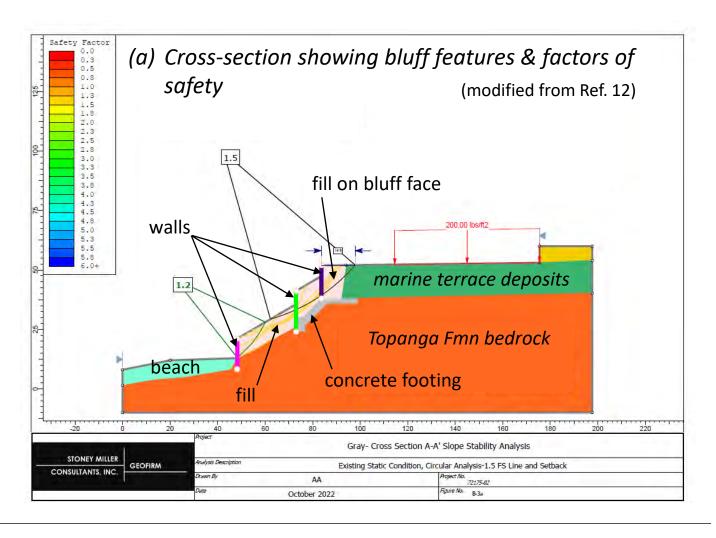
<sup>&</sup>lt;sup>3</sup> These relatively large distances result in part from measuring the 25-ft setback from all points and at all angles on the irregular bluff edge line (see Fig. 1).

Figure 1 – Geologic Site Plan with LUE Bluff Edge and 25-ft Setback

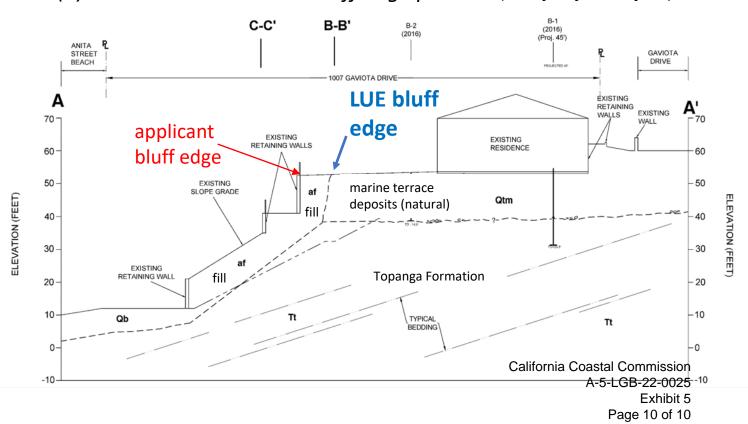


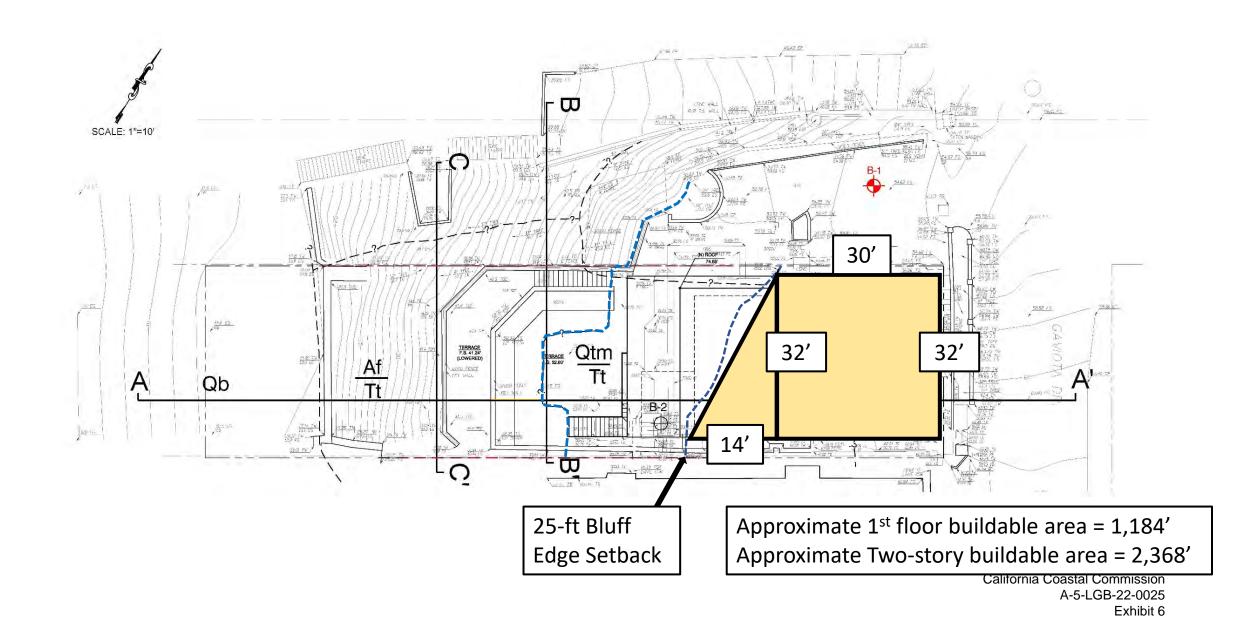
California Coastal Commission (modified from Ref. 13) A-5-LGB-22-0025 Exhibit 5 Page 9 of 10

Figure 2: Site Cross-Section (A-A')



# (b) Cross-section with LUE bluff edge position (modified from Ref. 13)





Page 1 of 1

CITY OF LAGUNA BEACH DEPARTMENT OF COMMUNITY DEVELOPMENT 505 FOREST AVENUE LAGUNA BEACH CALIFORNIA 92651

## **DEVELOPMENT REVIEW APPLICATION**

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# PERMIT DETAILED REPORT (RBP-2014-1270)

Permit Type Building - Residential

Work Class: Minor Remodel

Issued

Description: Remodel an existing SFR: Convert 151 sq ft

storage area to expand garage with new retaining wall at the rear east elevation; Remodel 980 sq ft. Lower Level - Reconfigure bathroom #3 and #4, add closet and shower to new bathroom. Main Level - Reconfigure existing kitchen, den and bathroom #2 into new kitchen, laundry and powder bathroom: Reconfigure existing master bathroom, closet, bedroom and bathroom #1 into a new master bath and closet. Includes grading of 38 cu yds

cut in garage area only per approved plans.

Project:

District: None

Square Feet: 0.00

Valuation: \$ 173,039.10 App Date:

07/14/2014

Issue Date: 08/06/2014

Exp Date: 02/02/2015

Final Date: NOT FINALED

Parcel: 644-076-01

Main

Address: 1007 Gaviota Dr

Laguna Beach, CA 92651

Main

Zone: R2 (Residential Medium Density)

Owner

Status:

Contractor

John Mcinnes

1007 Gaviota Drive Laguna Beach, CA 92651

Home:

Business: 949-500-0166 Mobile:

21761 Hermosa Ln

Trabuco Canyon, CA 92679

Home:

Business: 949-589-5999

Mobile: 949-584-1000

Applicant

933 Coast S Highway Laguna Beach, CA 92651

Home:

Business: 949-494-0476

Mobile: 949-338-2848

**Activity Type** E-mail

Activity Number Name

PMACT-001949-07-DEY - Ready

User

Grand Total for Permit

Melinda Dacey

Created On

7/31/2014 9:46:43AM

Requirements Prior to Permit IssBMA@T-001948-07-14Y

Melinda Dacey

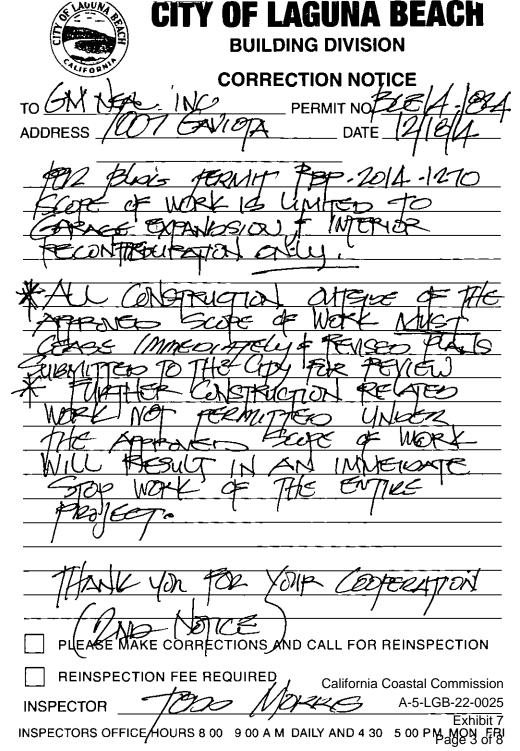
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00011270	Electrical Appliance Fee			Amount Paid
	Document Retention Fee		\$35.00	\$35.00
	Electrical Fixtures Fee	\$95.17	\$95.17	
	SMIP Fee - Residential (Category 1)		\$35.00	\$35.00
	Plumbing Permit Base Fee		\$22.50	\$22.50
	Electrical Outlets Fee		\$32.00	\$32.00
	Building Permit Fee		\$23.00	\$23.00
	Water Heater and/or Vent		\$2,180.47	\$2,180.47
	Fixture, trap, or set of fixtures on 1 trap		\$5.00	\$5.00
	Electrical Permit Base Fee		\$70.00	\$70.00
	Building Sewer		\$32.00	\$32.00
	Mechanical Permit Base Fee		\$32.00	\$32.00
	Building Permit Plan Check Fee		\$32.00	\$32.00
	SB1473-CBSC		\$1,417.31	\$1,417.31
			\$7.00	\$7.00
	Furnace or Burner up to 100,000 BTU		\$32.00	\$32.00
	Water Piping and/or Water Treating Equipment Exhaust Hood		\$70.00	\$70.00
			\$16.00	\$16.00
	Additional Appliance Vents		\$88.00	\$88.00
	Vent Fan Connected to Single Duct		\$77.00	\$77.00
	New Subpanel		\$21.00	\$21.00
	Gas Piping, 1-5 Outlets		\$25.00	\$25.00
		Total for Invoice 00011270	\$4,347,45	\$4,347.45

California Coastal Commission A-5-LGB-22-0025

\$4,347.45

\$4,347,45



City of Laguna Beach - Stop Work
Address 1007 GAV107A  Date: 12-12-14 Time: 3:32 a.m.p.m.  Permit #
Reason for the work order  CONSTRUCTION WELL BOSOND  THE APPROVED PLANS, PLANS  PEOL D FOR A NEW S.F. R.  Inspector NB. Complaint #

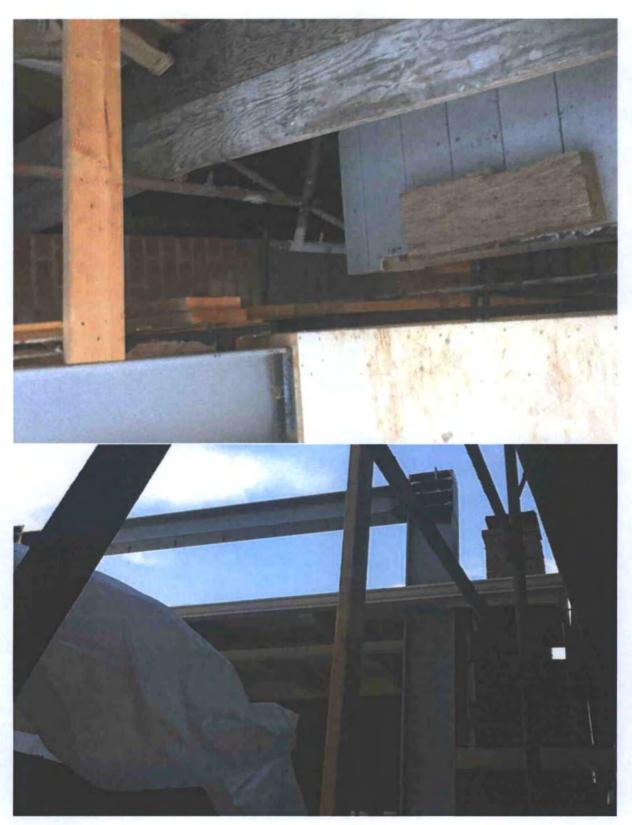


1007 Gaviota 12/18/14



1007 Gaviota

California Coastal Commission A-5-LGB-22-0025 Exhibit 7 Page 6 of 8



1007 Gaviota 12/18/14



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